



REVIEW

Perspectives of Vertical Axis Wind Turbines in Cluster Configurations

Ryan Randall¹, Chunmei Chen^{1,*}, Mesfin Belayneh Ageze^{2,3} and Muluken Temesgen Tigabu⁴

¹College of Automation, Qingdao University, Qingdao, 266071, China

²Center for Renewable Energy, Addis Ababa Institute of Technology, Addis Ababa University, Addis Ababa, 1000, Ethiopia

³BTeQ R&D Labs, Addis Ababa, 1000, Ethiopia

⁴Bahir Dar Energy Center, Bahir Dar Institute of Technology, Bahir Dar University, Bahir Dar, 6000, Ethiopia

*Corresponding Author: Chunmei Chen. Email: chunmei.chen@qdu.edu.cn

Received: 06 September 2024 Accepted: 19 November 2024

ABSTRACT

Vertical Axis Wind Turbines (VAWTs) offer several advantages over horizontal axis wind turbines (HAWTs), including quieter operation, ease of maintenance, and simplified construction. Surprisingly, despite the prevailing belief that HAWTs outperform VAWTs as individual units, VAWTs demonstrate higher power density when arranged in clusters. This phenomenon arises from positive wake interactions downstream of VAWTs, potentially enhancing the overall wind farm performances. In contrast, wake interactions negatively impact HAWT farms, reducing their efficiency. This paper extensively reviews the potential of VAWT clusters to increase energy output and reduce wind energy costs. A precise terminology is introduced to clarify ambiguous terms researchers use to quantify cluster parameters. While examining commonly studied and proposed VAWT cluster configurations, several aspects are discussed such as aerodynamic interactions, wake characteristics, structural dynamics, and performance metrics. Additionally, the current state-of-the-art and research gaps are critically described. The review also covers computational modeling, optimization techniques, advanced control strategies, machine learning applications, economic considerations, and the influence of terrain and application locations.

KEYWORDS

Vertical axis wind turbines (VAWTs); cluster configuration; wind farm; wind energy; performance enhancement

1 Background

During the past decade, a remarkable surge in the adoption of renewable energy sources has been witnessed. Reference [1] evaluated renewable energy development between 2012 and 2021. The global consumption of renewable energy rose from 480 to 1945 GW, and wind energy use grew by 562%, from 283 to 845 GW. Generally, wind energy conversion systems are classified based on the axis of rotation of the rotor, as either horizontal axis wind turbines (HAWTs) or vertical axis wind turbines (VAWTs). Research into VAWTs cluster aerodynamics is growing, encompassing rotor aerodynamics and inter-turbine wake interactions. Rotor aerodynamics studies are promisingly undertaken to improve the aerodynamic performance of VAWTs [2–4]. Several researchers used different strategies to enhance the overall performance of VAWTs. It has been found that the core of rotor aerodynamics is to have a high-efficiency turbine at low tip speed ratios and enhanced self-starting capability such as the studies of



[5–8]. Some of the strategies are presented here, Reference [9] proposed a novel hybrid Darrieus and modified-Savonius turbine to achieve an efficient turbine through a rotor aerodynamics study. Reference [10] implemented blade pitch to control the turbine blade which resulted in performance improvements, Reference [11] studied integrates the aerodynamic characteristics with that of the vibration characteristics used to investigate performance VAWTs by comparing with HAWTs.

On the other hand, the wake modeling deals with the flow fields downstream, the detailed review of available wake models is highlighted by [12,13]. The wake effect refers to an aerodynamic phenomenon produced by each turbine behind its rotor. Reference [12] demonstrate that due to the effect of dynamic stall, the wake aerodynamics of VAWTs are more complex than HAWTs. Because of the Magnus effect, which is described by [14], and deep dynamic stalls at windward, the wake of VAWTs demonstrates strong asymmetry in the horizontal direction. Using wake aerodynamics modeling, several researchers showed that HAWTs have higher efficiency as compared with VAWTs. However, this argument is valid when both turbines operate in isolation. It has been reported by several authors that arranging HAWTs in clusters leads to a decrease in performance, due to the turbulent wakes of adjacent wind turbines. The main issue with wakes is that it requires a large distance to fully recover, for this reason, it is necessary to install wind turbines as far as possible from one another. Spacing the turbines apart offers another notable benefit to reducing the fatigue load due to upstream turbines' turbulence. This results in the use of land which is most of the time not feasible. To avoid the effect of wakes, HAWTs in a wind farm need to be placed at least 20 rotor diameters (20D) apart in the downwind direction. Similarly, the study of [15] presented that for modern wind farms, HAWTs are typically spaced 3 to 5 rotor diameters apart in the cross-wind direction and 6 to 10 diameters apart in the stream wise direction. This arrangement aims to minimize aerodynamic interference between adjacent turbines. According to [16] the minimum distance required for VAWTs to recover the wake is about 6 times the diameter of the turbine. Furthermore, Reference [17] tests a hypothesis that arranging VAWTs in clustering can provide enhanced performance as compared with HAWTs. They verified that coupled configurations of counter-rotating VAWTs can provide improved performance. An appropriate arrangement of turbines in clusters plays a vital role in decreasing wake. Hence, it is possible to lower wake losses and raise the wind farm energy generation by considering this impact while placing the turbines.

The present paper explores the perspectives of using VAWTs in cluster configurations. This comprehensive review contains all aspects of vital information required for the clustering of VAWTs such as theoretical models, computational and numerical tools, optimization techniques, economic and market assessments, and other relevant aspects.

1.1 Review Methodology

The objective of the literature review is to determine and map research and project findings related to VAWTs in cluster configuration. The review aimed to provide insights into future perspectives to increase their global wind energy share with HAWTs. To examine the perspectives of VAWTs in the cluster configuration and identify key research gaps, a systematic literature review approach was adopted from the study of [18]. Synonyms for the following keywords were identified based on themes and terminology from a preliminary literature review: VAWTs, cluster configuration, and wind farm. The strings were used to search for titles, abstracts, and keywords of publications in Web of Science and Scopus. A total of 287 publications were found in the search, but after removing duplicates, 110 relevant ones were reviewed through abstract reading. Out of those, only 97 were systematically reviewed. Finally, 94 publications were found to be relevant and included in the final literature review. The review process of these 94 papers was based on a predefined protocol consisting of four themes: common cluster

configurations, computational modeling approaches and tools, optimization methods, and market and economics perspectives. Additionally, the performance comparison with HAWTs in cluster configurations was also reviewed.

1.1.1 Cluster Configuration vs. Wind Farm

According to a literature survey on the Scopus database, searching for VAWTs and cluster configuration, and VAWTs and wind farm as separate keyword combinations resulted in a different number of papers. The search returned 287 papers related to VAWTs and wind farms (see Fig. 1), and 56 papers related to VAWTs and clusters (see Fig. 2). It's worth mentioning that, during our search, we noticed that the term “wind farm” was more commonly used in the Scopus database as compared to the term “cluster”. However, these terms have been used by several authors to imply and convey similar meanings. In general, Figs. 1 and 2 show that the attention to VAWTs has significantly increased. In this study, a comprehensive review was conducted, including a total of 94 papers.

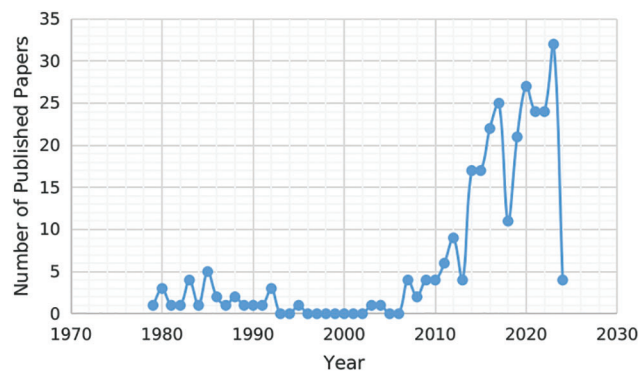


Figure 1: Number of published papers based on Scopus database with VAWTs and wind farm as search keywords

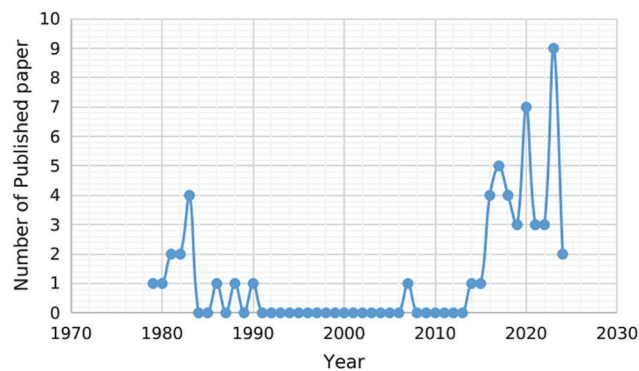


Figure 2: Number of published papers based on Scopus database with VAWTs and cluster as search keywords

1.1.2 Scope of the Review

The present review covered the state of research related to VAWTs cluster configurations and identified prospective research gaps in this area. It discussed several cluster configurations studied in the literature (Section 2), reorganized Section 3 into modeling and optimization, and experimental tests and

prototyping, presented findings from the experimental work (Section 4), provided insights into the market and economic aspects (Section 5), and some aspects of terrain and application (Section 6). The paper concluded by discussing key research gaps that require further investigation in this domain.

1.2 Terminology

To draw clarity among researchers' usage of different terms for VAWTs cluster, the following sections briefly defined cluster parameters. Fig. 3 describes the most commonly used terminology used in the study and optimizations of the VAWTs cluster configurations.

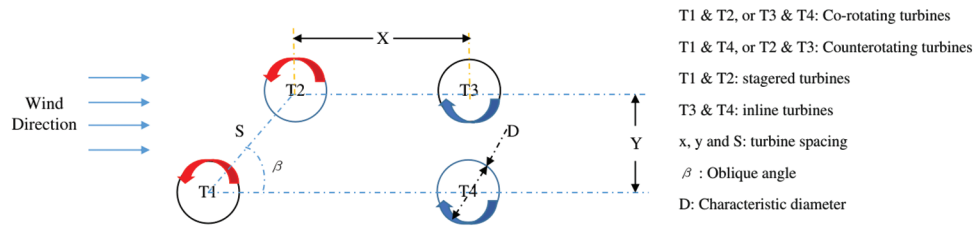


Figure 3: Cluster configuration terminology

To further elaborate on these terminologies, Table 1 is provided. The description provided in the table can be referred to better understand the specific meaning and context of these important terminologies.

Table 1: Common terminology used in cluster configurations of VAWTs

Terminology	Descriptions	Reference
Arrangement angles (Oblique angles or Angular arrangement)	The relative positioning of wind turbines in clusters. It is the angle between the line connecting the centers of two turbines and the wind direction	[19–21]
Blade pitch angles (BPA)	Angle between the chord line of the blade and the plane of rotation	[17]
Blockage ratio	The ratio of the turbine frontal area to the total frontal area of the farm. It depicted the flow blocked by the upstream turbines in a cluster	[22,23]
Characteristic diameter	It is the outer diameter of the rotor	[24]
Counter-down rotating turbines	The turbines are placed in a configuration where they rotate in opposite directions, along the wind direction	[25]
Counter-up turbines	The turbines are placed in a configuration where they rotate in opposite directions, against the wind direction	[25]
Tip speed ratio	The ratio of the blade tip tangential and the free-stream wind velocity	[24]
Turbine spacing (distance between turbines)	The distance between individual wind turbines	[26,27]

(Continued)

Table 1 (continued)		
Terminology	Descriptions	Reference
Wake decay	The gradual decrease in wind speed and increase in turbulence intensity within the wake of a wind turbine	[25,28,29]
Wake recovery	It is when the wind speed and turbulence levels within a turbine's wake gradually return to the free-stream conditions as the wake moves downstream	[12,19]
Wake contraction	It is the process when the wake of a wind turbine narrows in diameter downstream, due to the effect of surrounding air into the wake	[25]
Vortex shedding	The periodic formation and detachment of swirling vortices from the edges of wind turbine blades	[25,30]
Velocity wake	The reduction in wind speed downstream of a wind turbine, caused by the extraction of energy from the wind by the turbine	[19,25]

2 Cluster Configurations

A VAWT can be classified by several factors, including the alignment axis of rotation to the wind flow direction (cross-flow or vertical), and the blade orientation (straight, helical, curved) [31]. For this review, the main classification used is according to the type of force acting on the blades, i.e., drag force-based Savonius and lift force-based Darrieus. These types of turbines are commonly employed in the isolation or clustering of VAWTs due to their simplicity, fewer moving parts, and scalability when compared to other types of VAWTs. Recently, several VAWTs cluster configurations have been studied, to enhance the performance of the farm. Most of them are inspired by common geometry relations and bio-mimicry configurations of two or three VAWTs. The work of [32] demonstrates the implementation of bio-inspired configurations to VAWTs, they used Darrieus VAWT and their respective performance. Migrating birds and fishes can travel farther by positioning themselves at specific coordinates and gaining from the vortices shed by those ahead of them. Reference [25] reviewed different cluster configurations as the arrays of two and three VAWTs. They examined various parameters affecting the performance of clusters of VAWTs and presented a general guideline for selecting suitable values for each parameter in future research. However, the full implementation and realization of VAWTs in clusters still require substantial research. The clustering of VAWTs is a promising area, but several important concerns need to be addressed. In the spirit of this, the present reviews will provide substantial information and address different aspects of clustering VAWTs to further explore new possibilities. We have performed a thorough review of the existing clustering configuration suggested and studied by different authors. The findings of the review are summarized and briefly described in Table 2. The findings of the review are systematically summarized and briefly described in Table 2. This table provides a comprehensive exploration of various cluster configurations of VAWTs, detailing their rotational directions, configuration type, and schematics. Each configuration is presented with detail descriptions. Additionally, the schematics included in Table 2 visually represent the design and arrangement of each cluster, facilitating a better understanding of how these configurations function in practical applications. This structured overview not only highlights the diversity of VAWT designs but also underscores the potential advantages and limitations associated with each configuration, making it a valuable resource for both researchers and practitioners in the field.

Table 2: Review various cluster configurations of VAWTs

Ref.	Rotational directions	Number of turbines	Configuration type	Description	Schematics
[25]	Co-rotating, Counter-rotating along the wind direction, Counter-rotating against the wind direction, Co/counter-rotating	2	Co-rotating, Counter-down rotating, Counter-up rotating, Two staggered co-rotating up, Tandem, Two staggered co-rotating down	The Counter-down configuration generates more power due to stronger vortex interaction. While co-rotating configuration generates more power than counter-up configuration. Counter-down configuration is more efficient for both parallel straight-blade Darrieus and staggered wind turbines. For two largely spaced tandem wind turbines, the counter-rotating configuration showed better performance.	
[19,33]	Co-rotating wind turbines, counter-rotating, All co-rotating wind turbines Wind turbines rotate in the same direction and the opposite direction of the turbine	3	Triangular	Placing turbines nearby, it's essential to consider the flow created between them and how it interacts with the wind. However, for wider spacing, the primary factor is the direction of the wake deflection behind the upstream turbines. The induced flow and the wake deflection direction depend on the rotation direction of the turbines. For optimal results, a cluster with counter-rotating downstream turbines is best for smaller spacing, while co-rotating turbines are ideal for larger spacing.	
[34]	Counter-rotating	4	Four counter-rotating straight blade Darrieus wind turbines	It has been found that using small values of β (between 0 to 7.5 degrees) results in better cluster performance. This is because, for such small values of β , the impact of the wake coming from the wind turbines situated upstream on the ones situated downstream is minimal.	
[35]	Counter rotating	4×4 , 16×16 , and 32×32	Fish schooling	Compared to a single wind turbine, the power output of these configurations has significantly increased.	

(Continued)

Table 2 (continued)

Ref.	Rotational directions	Number of turbines	Configuration type	Description	Schematics
[36]	Co-rotating	7	Single column configuration of straight blade Darrieus wind turbines	The column generates 50% to 100% more power than a single wind turbine.	
[37]	Co-rotating	7 × 5	Column configuration of straight blade Darrieus wind turbines	Downstream turbines are more efficient than upstream turbines, for optimal farm layout.	
[38]	Counter-rotating	9	9 pairs of counter-rotating straight blade Darrieus turbines	The counter-down outperform the counter up configuration in power generation. Furthermore, the average power coefficient of each line decreases from Line 1 to 3, while remaining nearly constant from Line 3 to 5.	
[33]	Co-rotating	9	3 triangular shaped cluster co-rotating straight blade Darrieus turbines	The power density of a cluster of 9 turbines is 13 times greater than that of 9 isolated turbines.	
[26]	Co-rotating	27	27 pairs of co-rotating Savonius wind turbines	The power density of the wind clusters of 9 and 27 turbines are 7 times greater than 9 isolated turbines, and 4 times greater than 27 isolated turbines, respectively.	

(Continued)

Table 2 (continued)

Ref.	Rotational directions	Number of turbines	Configuration type	Description	Schematics
[39]	Co-rotating	8	2, 8 and 16 co-rotating Savonius wind turbines	Increasing the number of turbines and reducing the spacing between them can lead to higher power generation. For instance, increasing the number of turbines from 2 to 16 can increase power output by 19%. For the 8 turbines cluster, the efficiency of those in the middle of the column is better with larger turbine spacing, whereas those at the bottom generate more power when the spacing is smaller. The difference in power generation between top and bottom wind turbines is due to the direction of their rotation.	
[40]	Co-rotating and counter	Multiple	Aligned (see A), Staggered (see B), Staggered triangular clusters (see C), Staggered triangular clusters (see D)	It was discovered that wind farms with staggered triangular clusters with an angle less than $\phi < 90^\circ$ are more efficient. This is because the synergistic interaction between clusters results in improved power generation.	
[41]	Co-rotating and counter	Multiple	Planetary cluster	The optimal cluster resulted in an efficiency increment of 1.01% on the performance of the “sun” turbine in the planetary arrangement over the isolated turbine.	
[42]	Aligned collocated wind plant, Staggered collocated wind plant	Multiple	Collocating cluster of HAWT and straight VAWT	Aligned VAWTs and HAWTs upstream resulted in a 3.5% increase in power. Staggered arrangement caused a 2.6% decrease. Aligned configuration produces a similar wake to a traditional HAWT. A staggered configuration produces two interacting wakes that generate a more confined skewed wake.	
[43]	Mixed with HAWT and windbreaks	Multiple	Vertically staggered cluster of HAWT and VAWT	Both windbreaks and VAWTs aid in the recovery of the upstream wind turbine wake by facilitating the mixing of wind flow and reducing wind shear, thereby increasing the power output of VSWFs.	

3 Modeling and Optimization

3.1 Computational Modeling Approaches and Tools

One of the important topics in clustering VAWTs is the interaction between each turbine. Usually, this interaction is the most vital to optimizing and modeling the performance of clustered turbines. The wake interaction between turbines significantly determines the performance of the farm and the structural loads. Hence, the state-of-the-art aerodynamics modeling approaches for VAWT cluster configurations are examined in the following section. Furthermore, the review is extended to understand the structural dynamics of VAWTs under the influence of farm wake and turbulence.

3.1.1 Aerodynamics Models

To this end understanding the wake of each turbine is vital, which has led researchers to develop various methodologies for modeling it. There are various methodologies available to model the wake some of them are (1) analytical models such as the dipole model, top-Hat Wake Model, and actuator model, (2) computational fluid dynamics (CFD) which includes Reynolds-averaged Navier–Stokes (RANS) and large-eddy simulation (LES) methods, and (3) field measurements or wind tunnel experiments. The comparisons of different aerodynamics models are provided in [Table 3](#).

Table 3: Comparison of aerodynamic and flow characterization modeling tools for VAWTs in cluster

Model name	Approach	Accuracy	Reference
CFD methods:			
Reynolds-Averaged Navier-Stokes (RANS)	Averaging over time to obtain statistical mean values of variables	Moderate	[44]
Large-Eddy Simulation (LES)	Directly simulate large-scale turbulent structures	High	[45,46]
Detached-Eddy Simulation (DES)	Combine RANS and LES approaches in different flow regions	High	[45]
Unsteady Reynolds-Averaged Navier-Stokes (URANS)	Solve unsteady RANS equations to capture time-averaged behavior	Moderate	[20]
Analytical methods:			
Top-Hat wake model	Assume a simplified rectangular wake profile	Low	[28]
Gaussian wake model	Model wake using a Gaussian distribution	Moderate	[47]
Asymmetric Gaussian Wake Model	Model asymmetric Gaussian wake with varying parameters	Moderate	[48]
Actuator Line Model (ALM)	Represent blade aerodynamics using line elements	Moderate	[49]
Actuator Disk Model (ADM)	Account for average velocity deficit caused by turbine disk	Moderate	[50]
Vortex model	Represent interconnected vortices in the wake	High	[49]

CFD methods involve numerically solving fluid equations (such as Navier-Stokes equations) using computational methods, which provide a detailed representation of the flow field. The fidelity of CFD methods for the study of VAWTs are well presented by [51], they investigated seven eddy-viscosity

turbulence models to select the best-performing turbulence model. According to their findings, $SSTk-\omega$ is the recommended model to investigate the aerodynamics of VAWTs.

On the other hand, analytical methods simplify the wake behavior using mathematical formulations based on empirical correlations. They provide low computational cost insights into wake characteristics and are commonly used for initial assessments, conceptual designs, and quick estimations of wind farm performance. The relative performances of these models in terms of VAWTs cluster modeling have not been extensively explored. However, a brief review of recent computational research using these individual tools is discussed in the following sections.

One of the simplest analytical wake models used for VAWTs is proposed by [28] as the top-hat Wake Model. The model assumes the wake downwind of the turbine to have a rectangular form. The rectangular dimensions defined by H_w and D_w , which are defined by linear relationship as the wake is transported downstream, and can be expressed as;

$$H_w = H + 2k_{wz}x, \quad D_w = D + 2k_{wy}x \quad (1)$$

where the constants used to define the wake expand in the normal direction at the rate of k_{wz} and in the span-wise direction at the rate of k_{wy} .

Other wake models are based on continuity equation, conservation of momentum, and energy equation. Since the flow pattern in wind turbine applications is classified as low Mach flow, roughly 0.1 according to [52], the incompressible flow model is a good fit.

As the wind passes the turbines, it generates wake phenomena which have a negative effect on HAWTs farms. However, wake generation has significant importance in VAWTs clusters. To optimize VAWTs cluster layout, the wake effect must be modeled first. The wake effect is an aerodynamic phenomenon that occurs when each turbine creates a disturbance in the flow of wind that passes through its rotor. This disturbance causes the wind speed to decrease in the area behind the turbine, which results in less energy being extracted by subsequent turbines. By taking the wake effect into account when placing the turbines in the wind farm, it is possible to minimize wake losses and significantly increase the energy production of the wind farm. Several attempts have been made to model the flow characteristics of VAWTs in cluster configurations. The LES study of [45] for three different coupled configurations of VAWT for two values of tip speed ratio (TSR). Their finding demonstrated that the vortex interaction between coupled VAWTs wake is weak. However, the blockage effects play a significant role in creating a higher momentum flux downstream. This effect is more pronounced at higher TSRs, indicating turbines in staggered wind farm layout along the wind direction, can increase the momentum flux of downstream turbines. The aerodynamics study of VAWTs using CFD provides a powerful tool to study and visualize the details of complex wakes. There are three main modeling approaches these are RANS, LES, and DES. Hence, these aerodynamics models are used for the flow characteristics of VAWTs in clusters to provide clear insight for enhanced farm performance. The CFD investigation [53] using RANS $k-\epsilon$ model for cross-flow wind turbine for two type cluster configurations (1) aligned and (2) staggered configuration. Besides configurations, they also varied the distance between the turbine into three categories 0.5D, 1D, and 1.5D (D is the diameter of the turbine), and investigated the optimal distance between turbines within configurations. Their findings indicated that the optimal arrangement is staggered, and the closest distance between turbines can be 0.5D. In the wake zone, it is evident that the wind speed decreases, while the turbulence intensity increases, resulting in a high wind speed shear before downstream turbines. Hence, one of the advantages of a staggered layout is helps to reduce wake losses. The study of [54], used 2D CFD-simulation aiming to improve the power output from two different VAWTs in tandem arrangement. The simulation investigated the improvements by varying the array layout, rotational direction, and spacing. The authors provide a broader insight how the rotation orientation of the turbines as co and counter-rotating, the effect of turbine spacing, and the cluster layout. Their results indicated that pairs of VAWTs generated 15% more power than isolated turbines, and increasing the number of turbines

increased the overall efficiency. The hypothesis suggested for better performance of VAWTs clustering is the wake interaction. The detailed wake characterization done by [45] coupled configurations using LES. They found that the inter-turbine vortex interaction between wakes of coupled VAWTs is weak, resulting in improving performance compared to isolated turbines.

One of the common computational tools used in VAWTs cluster modeling is LES, for example [45] has done LES of three different cluster configurations of VAWT at two TSRs. The mutual vortex interaction between wakes of coupled VAWTs is determined to be weak. However, the blockage effects play a significant role in achieving an increased momentum flux of downstream turbines. This effect is more pronounced at higher TSRs, indicating that arranging staggered clusters can increase the momentum flux of downstream turbines.

The study of [43] on vertical staggered wind farms (VSWFs). The study found that both windbreak and VAWTs contribute to enhancing wake recovery of upstream wind turbines, leading to increased power output as shown in Figs. 4 and 5. The power generation rate of VSWFs increases with turbine spacing, and VSWF with VAWTs generates more power output than a windbreak. The height of the VAWTs significantly affects the power output, and the optimal configuration should not have an overlapping area or gap between the projection area of HAWT's and VAWT's rotors, i.e., blockage effect.

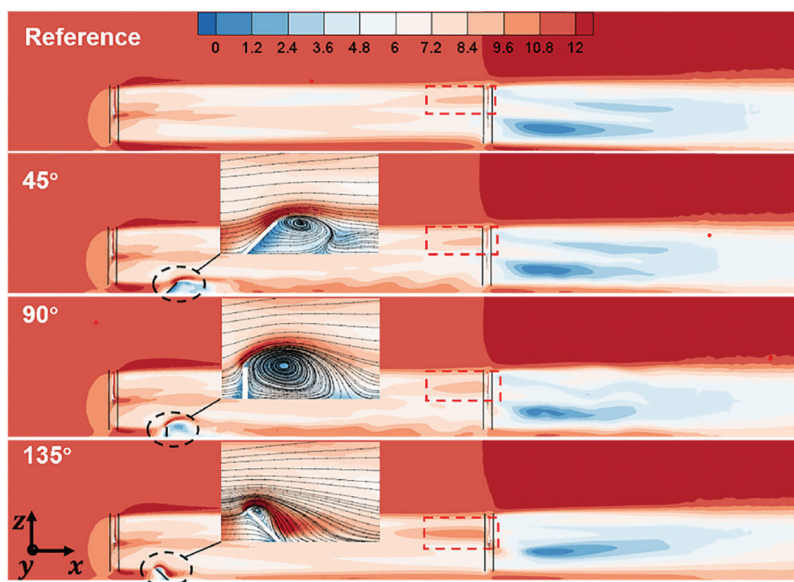


Figure 4: Streamwise velocity contour of aligned HAWTs with VSWF and windbreak for different tilt angles [43]. Adapted with permission from Reference [43]. Copyright ©2023, Elsevier

The study of [55] employed 2D URANS simulations to identify an optimal arrangement based on average turbine efficiency and area utilization efficiency. They have tested various arrangements that have been demonstrated to provide better performance, such as bioinspired layouts, and new and hybrid designs with several turbines. The capability of two-dimensional CFD analysis to accurately simulate the impact of the wake on the performance of different VAWT farms is explored by [44]. They investigated two H-Darrieus turbines using a commercial tool called STAR CCM+. The study demonstrated for the downstream of turbines that the wakes hold significant importance on the overall performance for a range of turbine spacing 2.5D to 40D. Using CFD and combining the ALM with LES to accurately investigate the effect of inter-turbine spacing and turbine rotation on the performance of VAWTs clusters have been studied by [49]. The ALM is one of the reduced-order models, and coupling it with LES makes it an effective tool for

analyzing wind turbine wakes. As compared with other reduced-order models, such as the ADM or Vortex Model, ALM is a more accurate model. The basic consideration of ALM model is the lifting surfaces of the turbine as actuator lines. Each actuator line is divided into several stations, as shown in Fig. 6a,b. The validation results showed the proposed tool determined wake characteristics properly and are in good agreement with the references. The study of [49] also investigated the effect of turbine spacing and rotations of three VAWT clusters. The proposed open-source tool demonstrated a robust framework for modeling and analyzing VAWTs, to comprehensively understand their performance and characteristics.

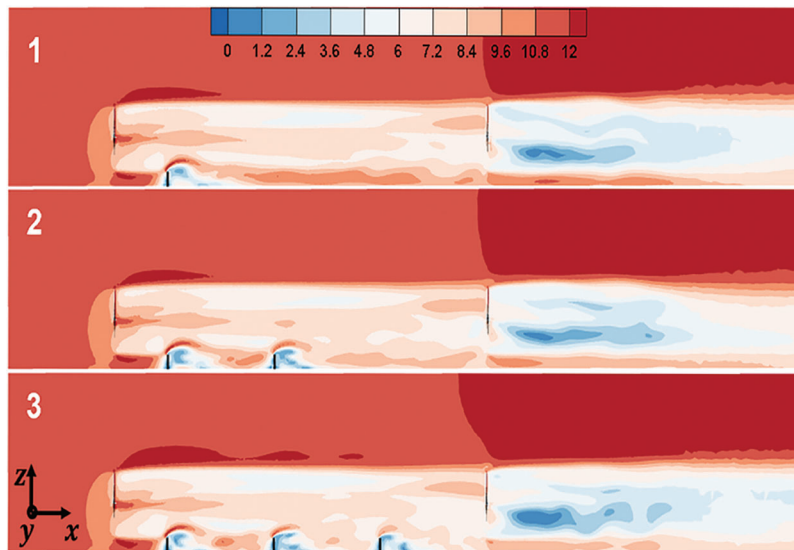


Figure 5: Streamwise velocity contour of aligned HAWTs and VSWFs with VAWT for different spacing [43]. Adapted with permission from Reference [43]. Copyright ©2023, Elsevier

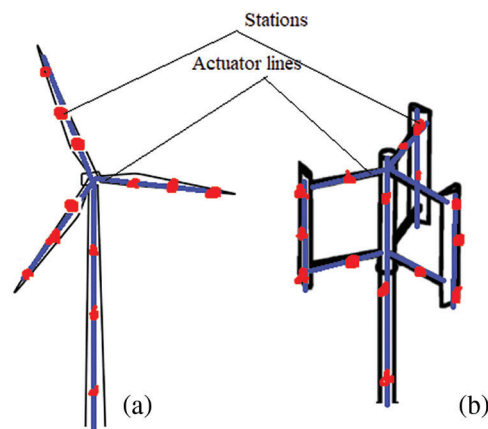


Figure 6: Schematics of ALM representation of (a) HAWT and (b) VAWT

In addition to the turbine spacing and rotational direction, other turbine characteristics have a significant role in the performance of farms. Reference [56] studied the effect of fixed and variable pitch control on the power coefficient C_p and mutual interaction between closely positioned VAWTs using 2D-CFD analysis, to

examine the power coefficient C_p for a range of TSR. The analysis indicates an enhancement in the performance up to 18%.

A series of CFD simulations, based on the two-dimensional 2D-URANS method, were performed on four arrangements of VAWTs clusters to achieve optimal power coefficient [20]. The study reveals that the average power generation is greatly influenced by the constraint effect in the lateral direction and the blockage effect of upstream turbines, which can be triggered at a specific separation distance. In most cases, a cluster of 3 VAWTs demonstrates a higher power coefficient compared to a cluster of two VAWTs. The configuration of three VAWTs—consisting of one upstream turbine and two downstream turbines—resulted in an average power coefficient improvement of up to 11.1% compared to that of an isolated turbine [20].

The efficiency of a planetary cluster design was studied using CFD simulations with a transient k-omega (SST) turbulence model. The use of “planet” turbines enhanced the efficiency of the central “sun” turbine by extracting power from the free stream. It has also witnessed an increase of 1.01% in the efficiency of the “sun” turbine of the planetary arrangement over isolated turbine [41].

Computational studies are further demanded to analyze tilted VAWTs for emerging applications such as high-rise buildings and floating wind turbines. It requires numerical validation of an existing experimental and computational work of VAWT in upright and tilted conditions. The correct parametric study for selecting the appropriate turbulence model and optimal computational parameters for solving the URANS equations, under constant TSR and tilted turbine conditions was demostarted by [22]. Their results indicated that SST k-omega captured the wake vortices better and closer to the experimental value than RNG k-epsilon model. Furthermore, based on the SST k-omega simulation, the wake of the tilted axis turbine proceeds downstream in a tilted manner. As a result, the wake stream shifts downward, and VAWT in tilted conditions produces higher torque downwind compared to the upright turbines.

The combined effects of different cluster parameters should also be investigated to provide comprehensive insight into VAWTs cluster development. According to the study of [57], the numerical simulation of twenty-two test scenarios on Savonius turbines in aligned, parallel, and oblique configurations using 0.25D, 0.5D, 1D, 1.5D, and 2D spacing. The power coefficient of backward two oblique turbines is determined to be twice higher than an isolated rotor. For three Savonius turbines arranged in optimal spacing, the average power output of the farm increased by a factor of 3. From this analysis, Reference [57] concluded that the average power output of a large number of Savonius turbine clusters will be proportional to the number of three turbine clusters.

The study of [19] employed CFD analysis to study the effect of spacing two turbines. Compared to isolated turbines, there was an improvement of 8.06% at a 2D turbine spacing, while a low improvement was seen at 12D spacing. The performances of 3 VAWTs in a pyramid- and inverted pyramid-shaped clustered configurations with varying oblique angles between 15° to 165° at a fixed spacing 2D were also investigated. For such configurations, the left-side and right-side turbines showed performance increase proportional to the oblique angle, except at 165°. Meanwhile, the center turbine achieved the highest performance at an oblique angle of 45°. The maximum cluster performance was achieved in the inline configuration and perpendicular to the wind direction, resulting 9.78% improvement of the overall performance over the isolated turbine [19].

The use of the ALM could significantly reduce the computational effort and cost of simulating VAWTs by modeling turbines as momentum source terms in the NS equations. ALM to investigate the synergy patterns within a cluster of two and three VAWTs employed by [58]. In conjunction with a URANS method using the SST k-omega turbulence model, the ALM has shown good computational accuracy in predicting VAWT synergy. The variation of the power ratio is characterized as a function of the cluster layout parameters, and the results show good agreement with previous investigations [58].

The study of [59] on the unsteady aerodynamics involved in the operation of VAWTs cluster using the actuator line model. The study involved a wide range of tip speed ratios (TSRs) and considered different inlet conditions such as uniform flow, logarithmic wind shear, and atmospheric boundary layer (ABL). The study also explored performance improvements through the deflected wake produced by the pitched struts of the upstream turbine. Numerical results were compared to experimental measurements, and the study found that the applied ALM could be considered as a potential tool for VAWTs studies, with relatively low computational cost showing accuracy and numerical stability. The study by [37] analyzed the flow structures and energy production of VAWTs arrays. The wake of co and counter-rotating VAWTs shows similarities with pairs of cylinders, and multiple turbines in a column increase power output due to regions of excess momentum between them. It also suggests that downstream columns can be more efficient than the leading column, potentially improving wind farm productivity.

3.1.2 Structural Loads and Dynamics

As VAWTs in cluster configuration are exposed to high turbulence and wake conditions, the structural reliability of the blades is an important factor affecting their safe operation. The detailed investigation of critical structural parameters on the aerodynamic performance VAWTs are provided by [60]. Hence, the structural safety of the turbines shall be examined for different load cases, mainly ultimate and fatigue strength due to steady and cyclic loads, and dynamics and flow-induced loads. As downstream turbines operate under extreme wake conditions, the effects of vortex shedding and flow-induced vibration should be quantified properly. When the frequency of the external load is close to the natural frequency of the structure, resonance will occur. Resonance will reduce the fatigue life of the structure and lead to blade failure. It will have a significant impact on the flutter limit of the blade, causing the VAWT blade to lose its aeroelastic stability.

Currently, research on the structural dynamics of wind turbine blades primarily focuses on HAWT. However, there are limited published documents regarding the structural dynamics of VAWT blades. Few efforts have been made to establish a VAWT dynamics model. For instance, Reference [61] considered the coupling effects between shaft bending, torsion, tension, rotor tension, and bending modes. Additionally, Reference [62] compared the connection method between the main shaft and blades of a 5 MW offshore floating VAWT to a cantilever beam model. Nevertheless, a comprehensive examination and quantification of the overall farm performance, as well as the interaction between structural dynamics and aerodynamic performance, are necessary to enhance farm output and extend the turbines's operational life.

A comprehensive computational analysis to study the wake interaction and the resulting aerodynamic loads exerted on the turbine blades was presented by [63]. The study investigates alterations in the normal and tangential aerodynamic loading across the blades of each turbine at various azimuth positions, see Fig. 7. Moreover, the radial and azimuth fluctuations in the aerodynamic blade loads play a crucial role in determining the magnitude of the rotor hub moments. These moments become particularly significant when there is an imbalance between the loads on the left and right sections or the upper and lower sections of the rotor. Reference [63] also showed for selected cases to indicate the variability of the loading and thus its fatigue driving potential. The analysis showed that the loading on the blades of the upstream turbine is highest when they are oriented upwards (90°) and lowest when pointing downwards (270°). The external loading is also determined to be nearly the same for the two horizontal positions 0° and 180° .

The load profiles of the downstream rotor exhibit notable variations depending on the specific flow conditions. Under full wake operation, the loads amplify as the turbulence level and turbine spacing increase. The blade loads at different horizontal positions display significant dissimilarities for laminar ambient flow and closely positioned turbines. Similarly, for laminar ambient flow and large turbine

spacing, a horizontal asymmetry is observed in the blade loads of the downstream rotor, see Figs. 8 and 9. Lateral displacement of the rotors affects the downstream rotor by the influence of the upstream wake. This leads to a decrease in average blade loading and an increase in standard deviation at a position of 0° . The presence of heightened turbulent mixing, resulting from ambient turbulence, causes an elevation in average loading on the blade at 0° . However, average loads on the blade in other directions experience a slight decrease as the turbulence level increases. The standard deviation of normal loads on the downstream turbine blades generally rises with higher ambient turbulence levels. In the scenario of full wake, there is only a minor difference in standard deviations between laminar inflow and an ambient turbulence intensity of 0.05. Limited meandering and organized vortex structures are potential explanations for this observation according to the work of [63].

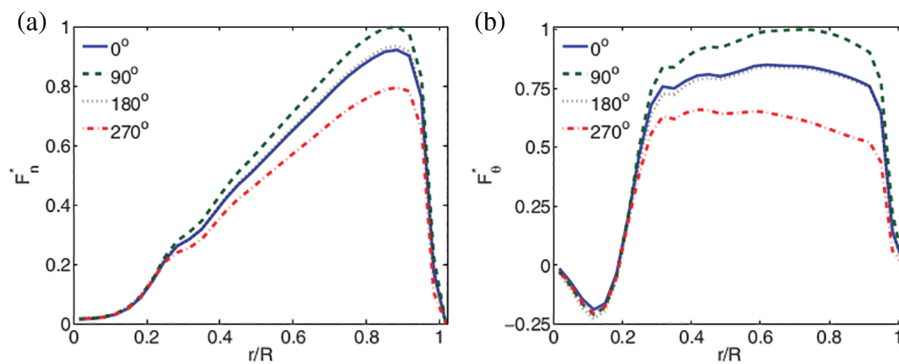


Figure 7: Normal (a) and Tangential (b) loads of the upstream rotor blade for different azimuth positions, $V_\infty = 8$ m/s and $[\text{std}(V_0)/V_\infty = 0]$ [63]. Adapted with permission from Reference [63]. Copyright ©2010, Wiley

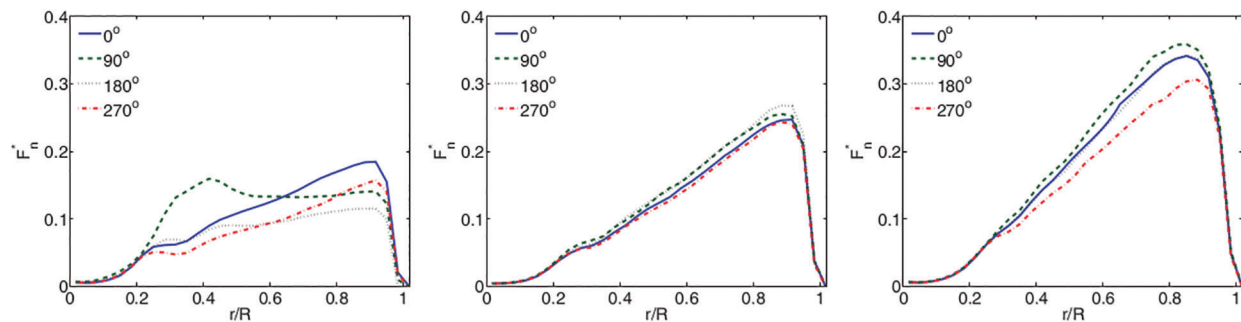


Figure 8: Downstream rotor blade span-wise normal load for different azimuth positions with the rotors stream-wise and lateral spacing $\Delta z = 3.3D$ and $\Delta x = 0$, respectively, and ambient turbulence intensity 0, 0.05, and 0.1, from left to right, respectively [63]. Adapted with permission from Reference [63]. Copyright ©2010, Wiley

3.2 Optimizations

Based on numerical modeling reviewed in the previous section, the performance of the VAWTs cluster is determined by several design variables, namely, rotational direction, turbine spacing, oblique angle, farm layout/pattern, wind direction, turbine types, number of turbines, tip speed ratio, blade pitch angle, flow-control methods employed, and wind shear profile. The optimal combinations of these variables are required to develop satisfactory VAWTs cluster configuration. There are two significant considerations for optimization. Firstly, the availability of limited land area for wind turbine farms necessitates optimizing the spacing between each turbine. Secondly, the arrangement of the turbines plays a critical role in their

performance, leading to the study of wake effects and the optimization of the arrangements of the turbines. To conduct the optimization study the most frequently used tool is computational study, while few records of using analytical and experimental studies have been found during the literature survey. One of the few pioneer research performed on full-scale field tests on VAWTs in arrays is the work of [17]. The work aims to provide a baseline for future research on computational and scale model experiments. During the field test, they used counter-rotating arrangements of VAWTs, they hypothesized that aerodynamic interactions between adjacent turbines can benefit the performance when nearby. The field tests used six 10-m tall by 1.2-m diameter VAWTs and were conducted with the turbines positioned within the same 75 m by 75 m tract of land. To optimize the best positions of array arrangement the following three sets were used in the field tests as shown in Fig. 10.

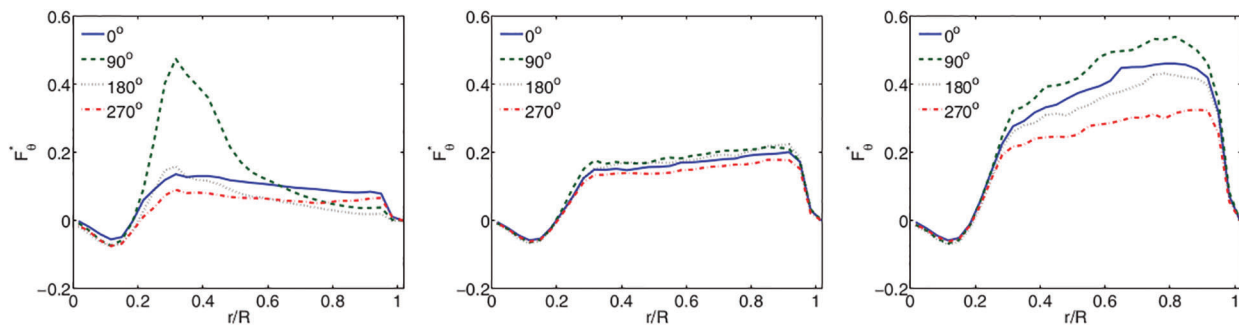


Figure 9: Downstream rotor blade span-wise tangential load for different azimuth positions with the rotors stream-wise and lateral spacing $\Delta az = 3.3D$ and $\Delta x = 0$, respectively, and ambient turbulence intensity 0, 0.05, and 0.1, from left to right, respectively [63]. Adapted with permission from Reference [63]. Copyright ©2010, Wiley

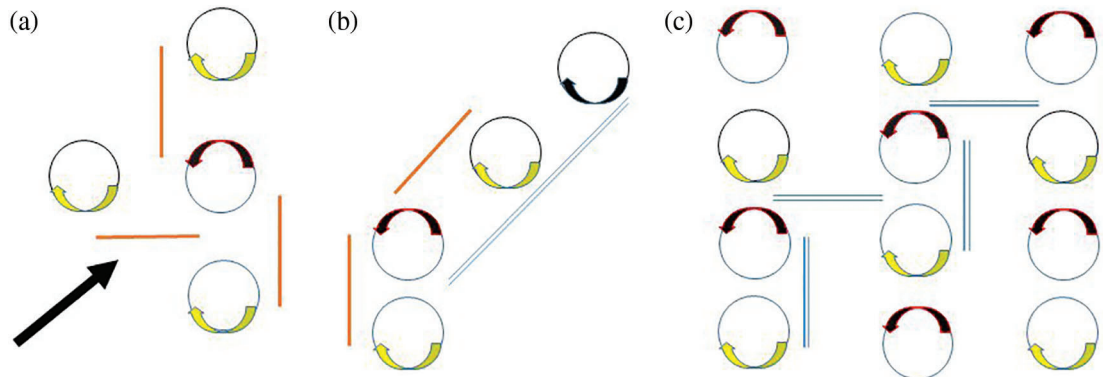


Figure 10: (a) Illustration of two-VAWT configurations. (b) Illustration of three VAWT configurations. (c) Illustration of six-VAWT configuration

Fig. 10a confirms that the proximity of the turbines slightly improved their performance relative to the turbines in isolation, Fig. 10b explored the effect of downwind blockage caused by the two closely spaced upwind turbines and a significant decrease in the performance of the downwind turbine was observed, and Fig. 10c demonstrates that increasing the spacing of all turbines in an array to $4D$ would be significantly reduced the upstream blockage effects. Based on their results, it is possible to improve power density by searching for optimal configurations for counter-rotating VAWTs.

A novel optimization methodology for VAWTs design proposed by [64]. The study investigates the self-starting behavior of adjacent rotors using CFD and a Taguchi-based design of the experiment approach. The optimized results demonstrated that the self-starting capabilities of each rotor are affected by modifications in the flow fields. Specifically, when the second rotor was positioned downstream from the center of the first rotor, it could not self-start due to momentum loss caused by the upstream rotor. However, with an optimized layout, the study achieved significant improvement in wake recovery downstream of the first rotor. Additionally, a substantial reduction in the wake extension for the first rotor was observed, which is beneficial for potential wind farm layouts. A 3D CFD simulations to examine the simultaneous impact of some layout parameters on the operation of two H-type straight-blade VAWTs was used by [65]. To discover optimal configurations, three design parameters were used: the direction of the incoming wind, the vertical distance between the mid-heights of two turbines, and the horizontal distance between the axes of the two wind turbines. It has been discovered that the paired wind turbines' performance is most affected by their vertical distance apart, while their power production is most influenced by their horizontal distance apart. Through their 3D simulation, it was discovered that the most optimal configuration for the turbines was achieved by placing them in a side-by-side arrangement, all at the same height. Besides vertical turbines working in air medium, they can also be deployed in tidal environments in clusters or as an isolated system. The work of [66] provides a useful insight clustering of Vertical turbines in tidal turbines. A 2D CFD study was employed to investigate the bidirectional Savonius tidal turbine to optimize the cluster arrangement and enhance the performance by using deflectors. To find the optimized deflector Kriging method (which is explained in [67]) combined with a genetic algorithm was used. The optimization study showed that the optimized cluster has a power coefficient improvement of 34.5% compared with the cluster without deflectors.

Determining the optimal spacing between clustered turbines is a critical parameter within the optimization process. To find optimized spacing, the study of [20] provides useful insight. The study follows a three-step approach to investigate the optimal spacing and power coefficient of clustered turbines. Firstly, a 2D CFD analysis is conducted using the URANS model for a single VAWT. Secondly, simulations are performed for various configurations including a single turbine, a parallel and staggered 2 VAWTs cluster, and a 3 VAWTs cluster facing the incident and leeward wind directions to determine the ideal spacing that maximizes the power coefficient. Lastly, the study examines the kinematic parameters of the ambient flow surrounding the turbine clusters to identify the mechanisms influencing the power coefficient. The findings confirm that, in general, clustered turbines exhibit superior average performance compared to isolated turbines when aligned with the prevailing wind direction. Specifically, the 3 VAWTs cluster demonstrates higher efficiency in terms of the average power coefficient compared to the 2 VAWTs cluster. For the 2 VAWTs cluster, the optimized spacing is determined to be around 1.5 to 1.6 times the turbine diameter, and the staggered arrangement proves to enhance performance due to the accelerated flow induced by the upstream turbines. Similarly, Reference [68] used the URANS equation to investigate the interaction between H-rotor Darrieus turbines in staggered wind farms and standalone clusters. It is found that the mutual interaction becomes negligible at a minimum distance of 13D.

Using analytical tools [69] develops a wake model of straight-bladed VAWTs and applies it to optimize the cluster configuration of VAWTs coupled with wind tunnel tests. The use of the wind tunnel tests is to determine the unknown parameters in the wake model. They have proposed a wake model and the schematic plot of the proposed wake model is shown in Fig. 11.

The model is based on the use of a continuity conservation equation, with a Cartesian coordinate system where the x-axis is pointing downstream, the y-axis is pointing windward, and the z-axis is aligned with the tower. A covariance matrix adaption-based evolutionary strategy (CMA-ES) was implemented to optimize the micro-siting of VAWTs using the wake model. The procedure of the CMA-ES algorithm for micro siting of VAWTs is shown in Fig. 12.

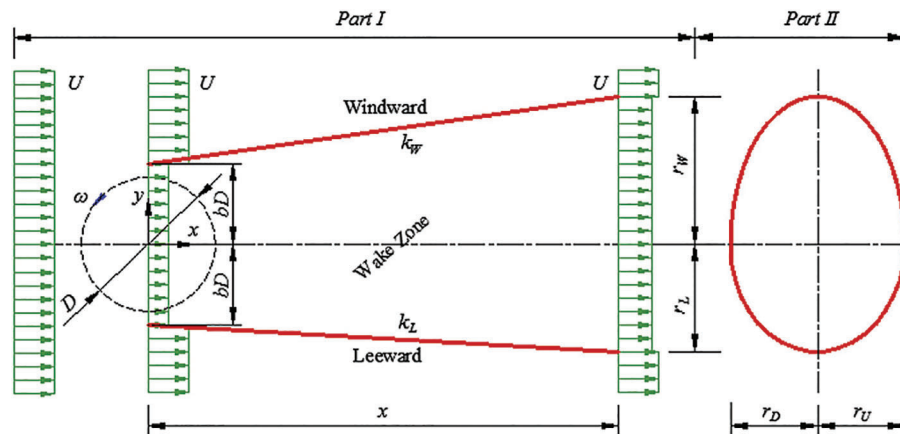


Figure 11: Schematic of the wake model of the VAWT [69]. Adapted with permission from Reference [69]. Copyright ©2017, Elsevier

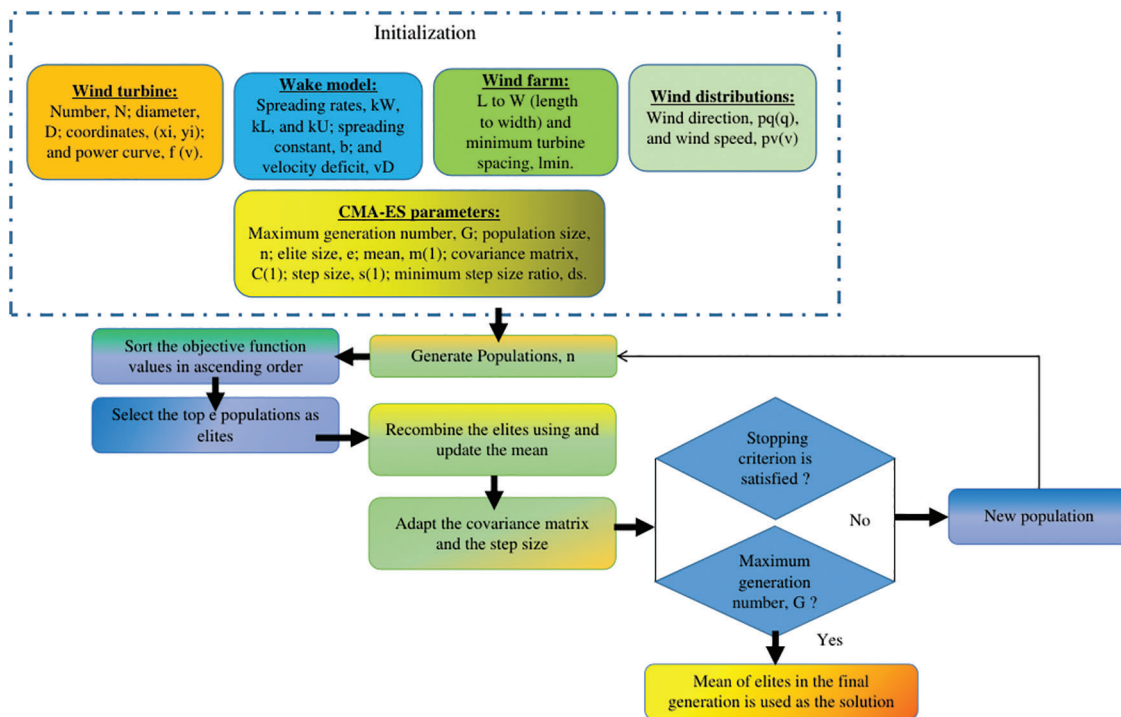


Figure 12: The procedure of the CMA-ES algorithm for micro siting

Other analytical models (top-hat model, the Gaussian model wake model, and Gaussian wake) coupled with experimental studies were used by [70] for layout optimizations. The utilization of wake models has enabled a comparison between layout solutions employing HAWTs and VAWTs within the same wind farm site. The findings indicate that in the wind farm layout optimization process, the energy density of VAWTs can surpass that of HAWTs, resulting in a more efficient utilization of sea areas. This is further enhanced by incorporating a layout optimization formulation that takes into account the direction of

rotation specific to VAWTs. By fully exploiting the asymmetric wakes generated by VAWTs, their potential is maximized within the wind farm layout.

Another benefit that comes from the wake interaction of VAWTs is their ability to improve the overall performance of HAWTs farms. To demonstrate this, Reference [71] used LES and analytical wake models to optimize the layout of HAWTs. The proposed strategy is to use small-scale VAWTs in triangular clusters deployed within a finite-size wind farm consisting of HAWTs. The clustering is shown in Fig. 13.

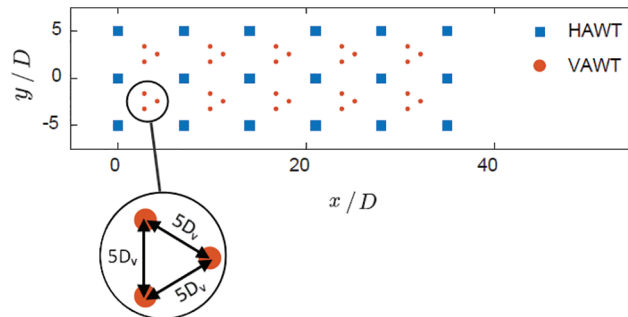


Figure 13: VAWTs clusters between HAWTs [71]. Adapted with permission from Reference [71]. Copyright ©2020, Purpose-Led Pulishig

According to the LES CFD analysis, VAWT wakes are visible far downstream of the farm because the wake behind VAWTs must expand enough vertically before it can be seen at the hub height of the HAWT. Because of the relatively wide relative distance between the two columns of VAWTs clusters, it is evident from Fig. 14 that the wakes of these clusters had almost recovered before the following column. When compared to the baseline scenario when just the HAWTs are present, they have discovered that the co-located wind farm's power output rises by up to 21%.

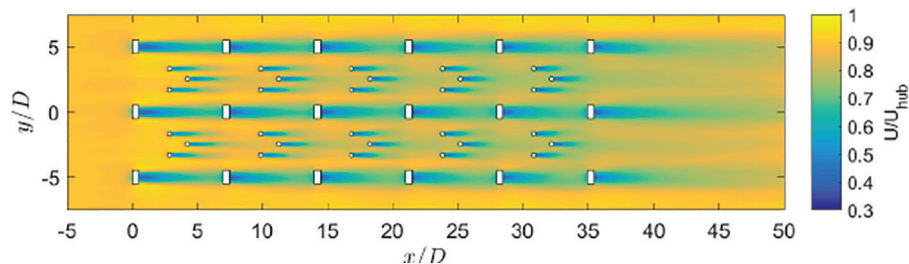


Figure 14: Stream-wise velocity of VAWTs clustered in HAWTs from LES [71]. Adapted with permission from Reference [71]. Copyright ©2020, Purpose-Led Pulishig

Furthermore, Reference [40] investigated the interactions of multiple VAWTs in small clusters, and subsequently used these clusters to design large VAWTs farms. For optimization, they have used the LES CFD model coupled with the actuator-line model (ALM-LES). They have performed the cluster design by geometric and shading considerations as shown in Fig. 15. The range of wind directions where two turbines can directly shadow one other is then enlarged by adding one more turbine. Nevertheless, depending on the direction of the wind, the third turbine could benefit from the increased wind speed created between the two upstream turbines, or the two downstream rotors may profit from the upstream

turbine's transverse flow deflection. By pairing these three turbines, they will be able to produce more power than from three distant, non-interacting turbines.

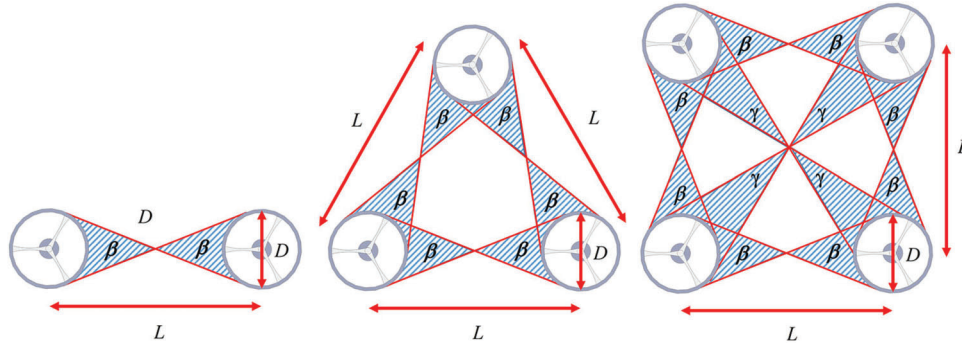


Figure 15: Two-, three-, and four turbine vertical-axis wind directions with upstream rotors [40]. Adapted with permission from Reference [40]. Copyright ©2018, Springer

To investigate the interactions between VAWTs to increase the wind-farm power density, Reference [40] have also performed the LES simulations of different cases. To visualize the differences in the flow patterns in these designs, the average stream-wise velocity component for a few selected configurations is shown in Fig. 16.

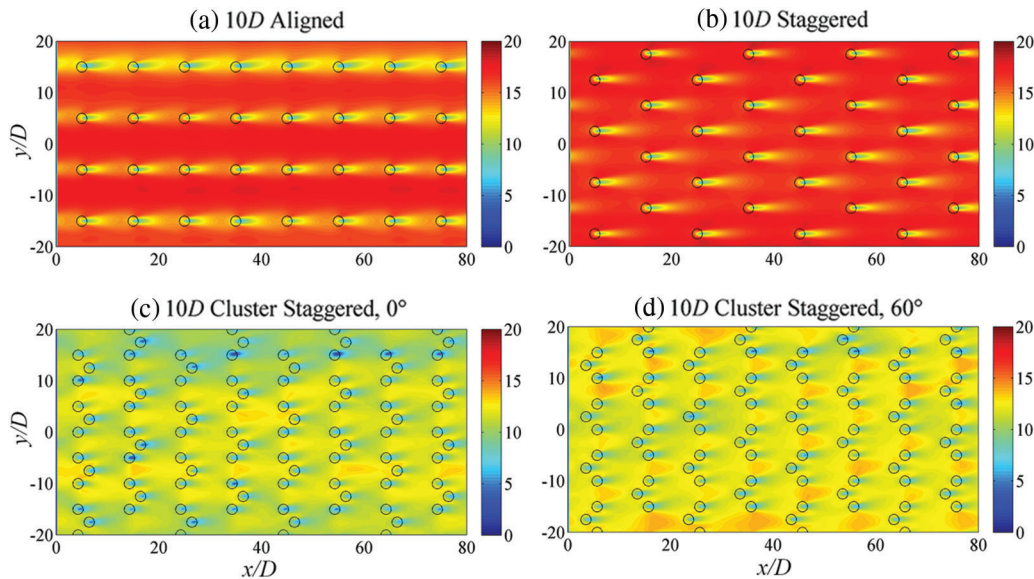


Figure 16: A 10D horizontal spacing wind farm with stream-wise velocity magnitude, mean flow from left to right: (a) regular aligned, (b) regular staggered, (c) cluster staggered with 0-degree wind direction, and (d) cluster staggered with 60-degree wind direction [40]. Adapted with permission from Reference [40]. Copyright ©2018, Springer

The simulations confirm that VAWTs, when arranged in well-planned clusters, positively impact one another: in such configurations, the power generation of a single turbine is increased by approximately

10%. Furthermore, compared to traditional setups, the cluster designs allow for closer turbine spacing, which results in almost three times as many turbines for a given land area. Using 2D CFD simulation [33] proposed an efficient way of clustering Savonius turbines. They have used the same geometric model arranged in three, nine, and twenty-seven to form a wind farm. They propose that the patterned Savonius VAWT farms, as shown in Fig. 17.

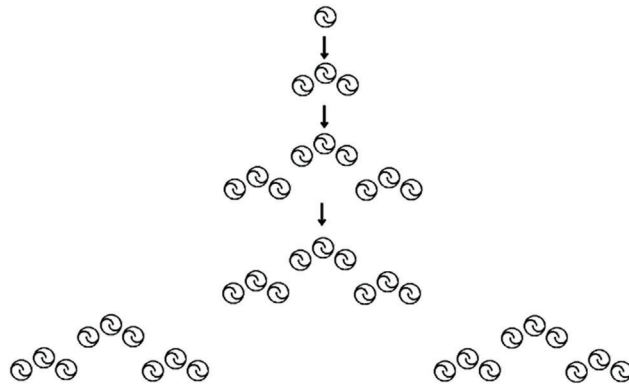


Figure 17: Farm development [26]. Adapted with permission from Reference [26]. Copyright ©2016, Elsevier

A similar study was performed for Efficient clusters and patterned farms for Darrieus wind turbines [33]. Their results of the simulation of the multi-turbine clusters are used to develop an efficient triangular shaped three turbine cluster having an average power coefficient up to 30% higher than an isolated turbine. A CFD study was performed for double Nautilus VAWT by [72] to optimize different layouts proposed, as shown in Fig. 18. They generally showed that the enhancement of the wind turbine arrays situation could significantly increase the average efficiency of the entire wind turbine cluster. The maximum average power coefficient reached 28.9%. Reference [73] also presents a variable-speed control method that provides an easy strategy to improve the power output of a cluster of turbines.

3.2.1 Optimal Configurations

Several cluster configurations have been studied for enhanced performance of the VAWTs farm. The most common optimal configurations are (1) collocated wind plants, (2) planetary clusters, (3) vertically staggered cluster, and (4) bio-mimicking blusters. Collocated wind plants are one of the promising cluster configurations is a collocated wind farm, wind farms with VAWTs are often staggered or aligned with the horizontal axis wind turbines to introduce clusters of VAWTs [42]. Collocated wind plant configuration encompasses three arrangements: (1) a typical wind farm with just wind turbines oriented horizontally, (2) an aligned collocated wind plant, and (3) a staggered collocated wind plant. In the collocated wind plants, clusters of three VAWTs are introduced to the standard wind farm and placed either in alignment with the horizontal axis wind turbines or staggered between the rows. Planetary cluster: according to [41], a new planetary cluster of VAWTs that can increase the efficiency and power density of wind farms. To conduct a parametric study and optimize this setup, the PCD (pitch circle diameter) and oblique angular, Φ , position of the smaller “planet” turbines were varied about the “sun” turbine. The “planet” turbines extract power from the free stream, which creates varied wind velocities and improves the efficiency of the central “sun” turbine. After conducting the study, it was found that the optimal PCD was 5D, and the best angular position for the “planets” was 30°. By comparing the “sun” turbine of the planetary arrangement to the optimum isolated, there was a percentage increase of 1.01% from 33.04% to 34.05%.

Additionally, an average improvement of 4% across the TSR range was discovered. Vertically staggered cluster: one of the major challenges in wind energy harnessing is to minimize the wake effect to enhance the power output of wind farms. To address this issue, windbreaks, and VAWTs have been added to traditional aligned wind farms, resulting in two innovative types of vertically staggered wind farms (VSWFs). Both windbreaks and VAWTs aid in the recovery of the upstream wind turbine wake by facilitating the mixing of wind flow and reducing wind shear, thereby increasing the power output of VSWFs. The power output of VSWFs with VAWTs is significantly higher than that of windbreaks. The layout optimization and effects of different parameters are discussed in [43]. Bio-mimicking clusters: the layout of the VAWTs cluster could also be optimized based on bio-inspired concepts. Reference [35] introduced an innovative VAWTs farm design inspired by the concept of fish schooling. They utilized the [74] potential flow model to study the wake effects of shed vortices on a school of fish. Inspired by the propulsion benefits of the reversed Karman vortex street observed in schooling fish, they utilized a similar configuration and modeling tools to analyze VAWT arrays. This approach produced optimal configuration results, resulting in a significant improvement in farm performance compared to isolated VAWTs and higher power density than HAWTs. Other bio-mimicking concepts could be employed to develop optimal farm layouts.

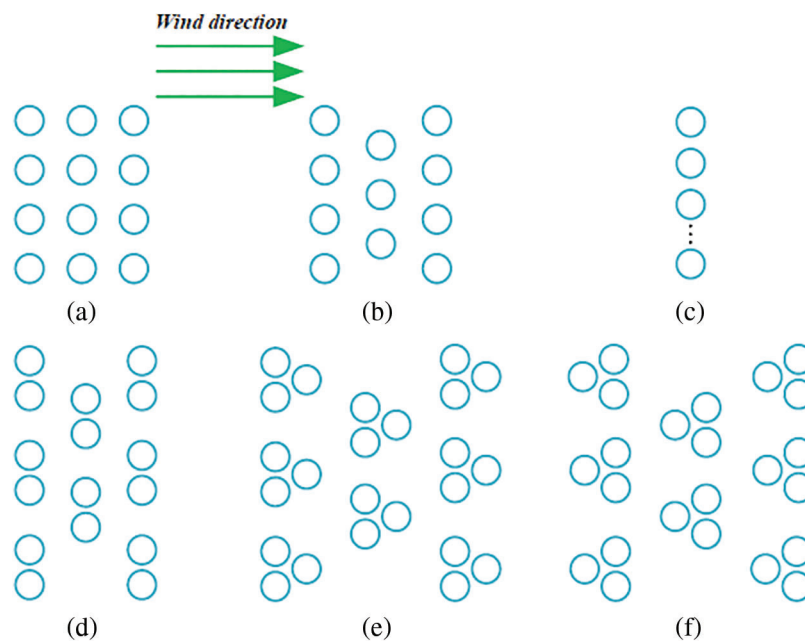


Figure 18: Different array layouts investigated [72]. Adapted with permission from Reference [72]. Copyright ©2023, MDPI

3.2.2 Application of Machine Learning and AI

In addition to advanced computational approaches, AI could benefit the optimization and enhancement of VAWTs cluster configurations. In this regard, in [75], a model has been developed that integrates three ensemble learning algorithms with clustering approaches to model wind power in a wind farm, using multiple meteorological factors. Ensemble models with clustering outperform models without clustering by approximately 15%, with the best-performing model using Farthest First clustering and improving by around 30%. Stacking fuses ensembles with varying clusters, further boosting power modeling

performance by about 5%. The proposed modeling framework is efficient, robust, and promising. Reference [76] suggested a unique method for combining data and knowledge to build the first digital twin of an offshore and onshore wind farm flow system that is capable of predicting the spatiotemporal wind field *in situ* over the whole wind farm. Through the use of physics-informed neural networks, the digital twin is created by combining the Lidar observations, the Navier-Stokes equations, and the actuator disk technique of turbine simulation. The architecture allows the merging of flow physics to retrieve unmeasured wind field information and the smooth integration of Lidar observations and turbine operating data for real-time flow characterization. As a result, it overcomes the shortcomings of current supervised machine learning-based wind prediction techniques, which are unable to make such predictions due to a lack of training objectives. The digital twin accurately mirrors the physical wind farm, capturing detailed flow features. Case studies have exhibited this. It also has a low prediction error of 4.7% for flow fields, enabling new research for wind farm life-cycle monitoring, control, and load assessment. There is a great deal of effect that wake interactions have on a wind farm's overall performance. A novel deep learning method, called Bilateral Convolutions Neural Network (BiCNN), is proposed and then employed to accurately model dynamic wind farm wakes based on flow field data generated by high-fidelity simulations [77]. As opposed to the current machine-learning-based dynamic wake models, which depend on dimensionless reduction, the suggested BiCNN is made to directly process various input kinds via background and foreground paths, thereby eliminating dimensional reduction errors. Significant findings demonstrate that the created machine learning-based wake model can accurately forecast wakes in real-time; that is, it can run at the same speed as low-fidelity static wake models and capture the spatial fluctuations of dynamic wakes in a manner akin to high-fidelity wake models. Regarding the free-stream wind speed, the derived model's overall forecast error is 3.7%. Moreover, the outcomes for a test farm with 25 turbines demonstrate that the created model can forecast the dynamic wind farm wakes in a matter of seconds [77]. The work of [78] demonstrated the application of machine learning for predictive maintenance of wind turbines and they proposed a revolutionized the way wind energy systems are maintained.

3.2.3 Control Strategies

The common control principles employed in VAWTs to benefit the cluster performance are Variable swept area (VSA) as smart rotors [79], rotation direction [49], TSR [80], Variable pitch controller [56], and through the application of active flow controllers such (i) surface blowing or suction, (ii) VG's, surface heating, plasma or (iii) changes in section shape (aileron, smart materials, and micro-tabs) [81–83]. Furthermore, the application of AI and machine learning as smart controllers will enhance the farm performance. Reference [79] employed a Fuzzy Logic Controller (FLC) to vary the turbine's swept area, which is adjustable for height and width with actuators. The VSA rotors are controlled by an FLC to maintain a constant power rating at the PMSG. Furthermore, the change in the turbine swept area will then alter the downstream flow characteristics. In a general sense in existing studies on VAWT arrays, little attention is paid to the real-time control of individual rotors in VAWT arrays. In arrays, the pitch control curve for VAWT in different positions should change due to the interaction of adjacent turbines. References [58,84] explored the dynamic pitch control strategies in double-VAWT arrangements. Pitch control enables the downstream rotor deviating from the wake ($\Psi > 15$) to fully utilize the flow acceleration adjacent to the upstream VAWT. With upstream pitch control, downstream rotor efficiency can also be improved see Fig. 19. The primary causes of the changes and improvements in the flow and the effectiveness of the VAWTs in the configurations are the decrease in the rotor's blockage effect and the acceleration of the wake brought on by pitch control.

In addition, other wind farm control principles used in HAWTs farms could be adapted for VAWTs clusters. For instance, the recently proposed collective wind farm operation and control based on a

predictive model by [85], could be employed for VAWTs clusters to collectively control all the turbines within the farm for a synergized farm operation.

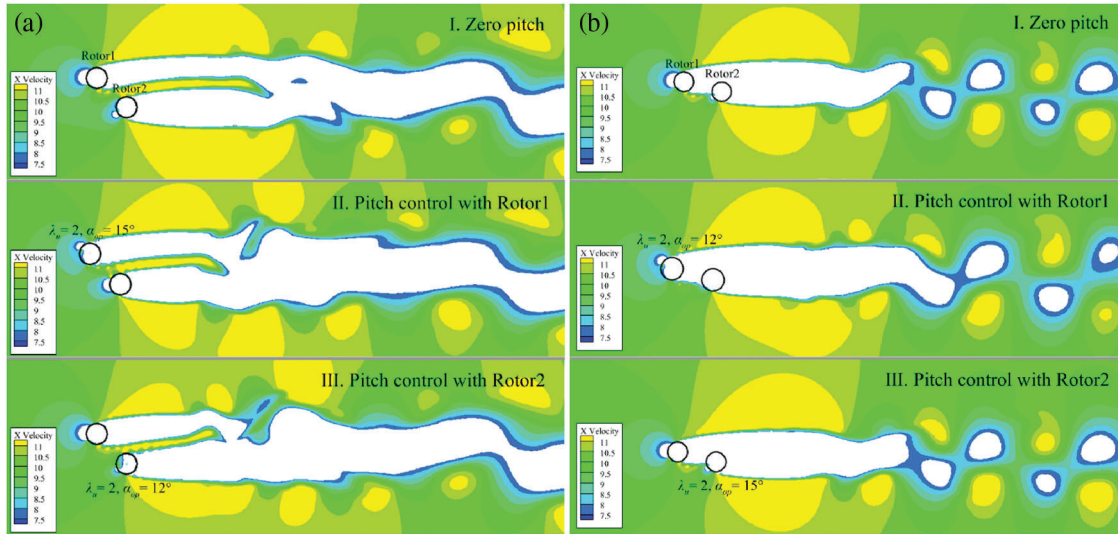


Figure 19: Wake development of the VAWTs in arrays under different control strategies ($\lambda_1 = \lambda_2 = 2.0$): (a) $\Psi = 45^\circ$ (b) $\Psi > 15^\circ$ [84]. Adapted with permission from Reference [84]. Copyright ©2023, Elsevier

4 Experimental Tests and Prototyping

Alongside analytical and computational studies, experimental tests and validations are essential. To examine the performance of VAWTs in cluster configurations, few experimental studies have been done. For example, experimental study of wake evolution under vertical staggered arrangement of wind turbines of different sizes are presented by [86] with the experimental setup shown in Fig. 20 and the measurements made by [87] showed the wake from lift-driven VAWTs in a wind tunnel and compared the results for three counter-rotating and isolated versions. They discovered that the wake of a paired VAWT is greatly influenced by the direction of rotation and that the wake of an isolated VAWT is deflected. The length, breadth, and replenishment of the wake of a counter-rotating VAWT that has adjacent blades moving downwind are comparable to those of an isolated VAWT. The wake of a counter-rotating VAWT with nearby upwind moving blades, however, is very different from the wake of an isolated VAWT in terms of replenishment and breadth. Paired VAWTs provide distinct benefits for wind farm applications because of their attractive wake characteristics, particularly for offshore floating wind farms. In another study, Reference [88] conducted an experimental investigation to explore the interactions between VAWT's rotor and wake. By considering various wake deflections, they evaluated the interactions, taking into account the pitch angles of the upwind VAWT's blades. Using stereoscopic particle image velocimetry, they examined wake interactions between two VAWTs in nine different wake deflection and rotor position combinations. Additionally, force balances were employed to assess the time-average loads on the VAWTs. The study findings confirmed the effectiveness of wake deflection and quick wake recovery, ultimately enhancing the available power of the second rotor.

The work of [89] showed a thorough investigation using wind tunnel tests to determine how the arrangement of the array affects VAWT power performance. When the transverse spacing is 2.4 rotor diameters, the maximum power coefficient of the turbine pair is 8.2% greater than that of an isolated turbine. The ideal mode of the transversal arrangement is counter-forward rotation. In the two-turbine and three-turbine longitudinal layouts, the maximum power coefficient of a downstream turbine is found to be

enhanced by 45% and 61.1%, respectively, in comparison to an isolated turbine. The proposed design includes trusses and triangles depending on the direction the wind is blowing. The experiment's outcomes verified that by fine-tuning the turbines' array arrangement, the average power coefficient may be raised even higher.

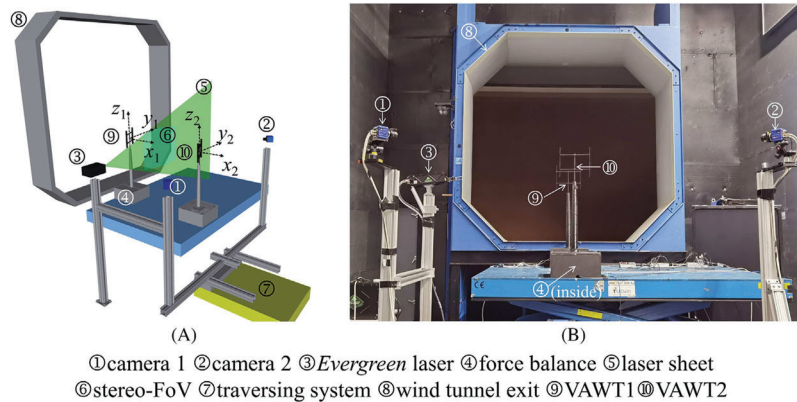


Figure 20: (A) schematic of the experimental setup; (B) a snapshot of the setup [88]. Adapted with permission from Reference [88]. Copyright ©2023, Wiley

5 Market and Economics

In addition to the aerodynamic performance of VAWTs in a clustered configuration, it is important to evaluate their financial feasibility under various scenarios. Although the technology for horizontal wind turbines (HAWTs) is advancing rapidly and driving down costs, it may be possible to further decrease the cost of offshore floating wind by opting for VAWT technology. VL Offshore has developed a cost-effective 5 MW floating foundation, known as the Y-Wind semi, for HAWTs [90]. To compare the Levelized Cost of Energy (LCoE) of the Y-Wind semi with a 5 MW HAWT against the same foundation with a 5 MW VAWT, a 200 MW wind farm located approximately 10 km offshore the Northeast U.S. at a water depth of 100 m was considered for bench-marking. The LCoE results indicated that a foundation for a 5 MW VAWT will be more commercially viable than a comparable foundation for a 5 MW HAWT. These LCoE values compare favorably to most electricity prices in the Northeast states [90].

The technological advancements have reduced a variety of capital, operational, and financial cost categories, resulting in a regional diversity in LCOE was examined by [91]. Due to the variable geospatial features of the farm sites under consideration and the nonlinear dependence on these input parameters, a specified change in the cost of a single turbine subsystem produces a range of LCOE outcomes; for instance, a 10.8% improvement in net capacity factor can reduce LCOE by between 6% and 20% at different sites [91]. Hence, technical innovations can have a significant influence and should be taken into account both spatially and temporally when funding or prioritizing technology innovation research to enhance offshore wind technologies. Through the analysis conducted by [92], the impact of varying spatial characteristics in the U.S. offshore wind resource area on the LCOE and economic feasibility of offshore wind was quantified. The report takes into consideration current technology, market, and regulatory conditions and presents a cost-effective option between fixed-bottom and floating offshore wind technologies for different site conditions while also evaluating the impact of technology advancement and market maturity. The results of the study suggest that offshore wind can potentially achieve significant cost reductions and forecasted economic viability in select regions of the United States within the next 15 years [92].

In general, the factors commonly considered in calculating LCoE include Capital Cost, Operating Lifetime, Capacity Factor, Fixed O&M cost, Variable O&M cost, and Electricity Price [92]. To reduce LCoEs for Wind Farms, advancements in turbine and blade technologies should continue to increase power output, improve efficiency, and decrease costs. Additionally, optimizing the spacing of individual wind farm units could also help reduce LCoE values. Further research may uncover ways to minimize down turbine wake effects, increase capacity factor, decrease in-field cable lengths, and improve power output by spacing VAWTs closer together [38,90].

6 Terrain and Application Locations

6.1 Noise Generation

All rotating machines inherently generate a significant amount of sound, which affects the vicinity. The application of most types of machinery depends on sound pollution. Several studies indicated that VAWT is more silent than HAWT in comparison. Reference [93] provided LES and aeroacoustic spectra for three configurations of increasing flow complexity: a nearby farm of four vertical axis turbines (that have the same characteristics as the isolated turbine), an isolated rotating VAWTs made up of three rotating airfoils and an isolated NACA0012 airfoil. Only the blade passage frequency and the boundary layer tones can be distinguished when comparing the spectrum with the isolated turbine. The aeroacoustic footprint of nearby VAWTs cannot be adequately described by a linear combination of sources from isolated turbines, as indicated by variations in acoustic amplitudes, tonal frequencies, and sound directives. Rather, farms should be viewed and investigated as distinct entities. This will benefit VAWTs for application in urban and rooftop applications and other sound-constrained sites.

6.2 Onshore vs. Offshore

One important new source of clean, renewable energy is onshore wind power. However, onshore wind does have certain limitations. It is hard to locate wind-generating projects in heavily populated areas like the Northeast of the United States. Because of this, any onshore wind farms will need to be situated farther out, which will present more logistical and transmission difficulties, along with increased costs and power loss. One of the promising solutions is to install floating wind power offshore. Offshore wind offers proximity to large population centers, a vast and more consistent wind resource, and a scale-up opportunity. On the other hand, offshore wind suffers from high LCOE and, in particular, high balance of system (BoS) costs owing to accessibility challenges and limited project experience. Preliminary studies on offshore VAWTs clusters showed their significant economic feasibility [90,94]. As discussed in the section (market and economics), the comparison between offshore HAWTs and offshore VAWTs clusters indicated that VAWT will be more commercially viable than a comparable foundation for a 5 MW HAWT [90]. Fig. 21 summarized the work of [94], they explored cost trade-offs within the design space for floating VAWTs between the rotor and platform configurations and corresponding performances. The benefit of a floating VAWT is envisioned through system-level improvements and balance of system (BoS) cost reductions, which are addressed in this project through design studies that feed into an LCOE analysis.

As per [94] the Darrieus rotor is a VAWT rotor configuration proven with field experience and offering structural advantages and aerodynamic efficiency similar to a HAWT. However, there is still room for enhancement of the Darrieus rotor when designing VAWTs at large scale and for floating offshore systems.

6.3 Urban Environment

In addition to the low noise generation benefits of VAWTs, their characteristics under wake conditions make them a promising source of energy in urban areas. Urbanization leads to more high-rise buildings and raises questions about their impact on wind flow and energy potential. Matching wind turbine performance with local conditions is essential for efficient power output in buildings and urban areas.

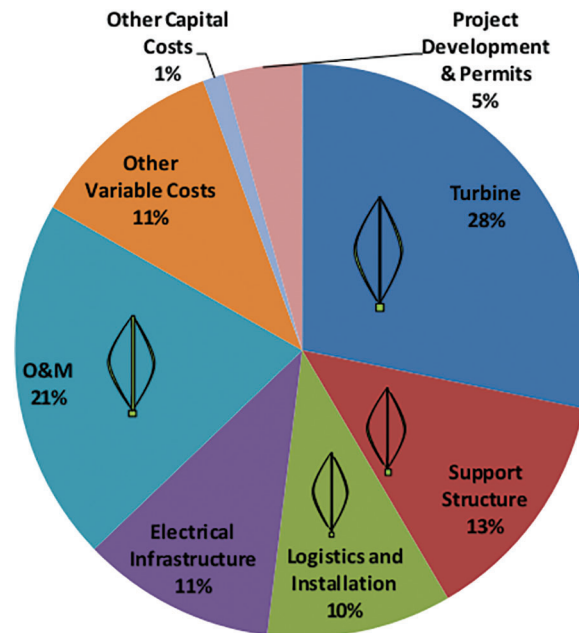


Figure 21: Estimated life-cycle cost breakdown for an offshore VAWTs [94]. Adapted with permission from Reference [94]. Copyright ©2016, Purpose-Led Publishing

According to the study of [95], the wind characteristics and the interference effects around high-rise buildings based on the level of building exposure to the wind and the position of surrounding buildings. They also determined the wind energy resource above the roof in terms of the Wind Power Density (WPD), turbulence intensities, and skew angle. The analysis forecasted high turbulence and skewed flow in urban areas were found to affect their efficiency and operability, which indicates the suitability of VAWTs in such conditions.

The study of [96,97] offered viewpoints on the study of wind energy from the construction and urban aerodynamics standpoint. They reviewed the recent designs of urban/building-based wind energy systems, such as building integrated VAWTs, power windows, wind-induced vibration-based wind energy harvesters, double skin, and other creative building facade systems, and wind source exploration. They also examined factors affecting urban wind flow and the effects they have on urban wind energy harnessing.

6.4 Comparison with HAWT

In the previous sections, several configuration of the VAWTs cluster were addressed. Their comparative advantage against HAWTs shall be identified to provide clear insights. Several studies compared the performance and characteristics of HAWTs and VAWTs in cluster configurations. The common comparison criteria considered are, LCOE, aerodynamic performance, power density, aerodynamic loads, complexity, and noise, to mention a few. Table 4 discusses the few types of comparative research between equivalently rated VAWTs and HAWTs. Table 4 discusses the few comparative types of research between equivalently rated VAWTs and HAWTs. This table provides findings from multiple case studies, highlighting the distinct performance characteristics of each turbine type. The analysis reveals that VAWT clusters exhibit significant advantages over their HAWT counterparts across a wide range of performance indicators. Based on the case studies reviewed, VAWTs clusters showed a promising advantage over HAWTs through wide areas of performance indicators.

Table 4: Performance comparison of cluster of HAWTs and VAWTs

Reference	HAWTs description	VAWTs description	Tool used	Comparison criteria	Results
[98]	2–6 MW HAWT	3 Bladed Darrieus (H-type) and Troposkien ϕ -type rotor configuration	CFD	Aerodynamic performance	VAWTs not only have superior performance but also feature a simple and cost-effective design for manufacturing and maintenance.
[90]	200 MW Floating HAWT farms	200 MW Floating VAWT farms	Analytical	LCOE	The LCOE values compare favorably to the LCOE values for most electricity prices in the Northeast states.
[99]	200 kW HAWT	200 kW VAWT	CFD	Noise	The comparison with an equivalent horizontal axis wind turbine operating at optimum tip speed, indicates a noise emission at the absolute bottom of the range.
[55]	Three identical in-line HAWTs using a spacing of 3D	Three identical in-line VAWTs using a spacing of 3D	CFD	Aerodynamic performance	For VAWTs clusters, the C_p are determined to be 0.462, 0.121 and 0.088, for the leading, second and third turbine, respectively.
[54]	Vestas V80 turbines with a rotor diameter of 80 m and a hub height of 70 m, are arranged in six columns and three rows in the streamwise and lateral directions, respectively	Collected 200 kW turbines, which are the three and straight VAWTs with a diameter of 26 m, the blade span of 24 m, and the height of 40 m, in triangular clusters in the free space among HAWTs	LES and analytical model	Power gain	The potential power gain in the wind farm with both HAWTs and VAWTs is up to 21% compared to a baseline case in which only HAWTs are present.
[100]	Large HAWT, the RE-power 5 MW model, placed at $x = 500$ m and $y = 250$ m,	Each HAWT is surrounded by 20 small VAWTs (H or Giromilltype) with a capacity of 50 kW and evenly distributed in a vertical staggered arrangement	The HAWT is parameterized with the ALM, while VAWTs use the ADM 1	Power output	The VS wind farm produces up to 32% more power than the traditional one, and the power extracted by the large turbines alone is increased by 10%, caused by faster wake recovery from enhanced turbulence due to the presence of the small turbines.

7 Conclusion and Recommendations

The present paper comprehensively examined the perspectives of VAWTs in cluster configurations. The review identified several promising VAWTs cluster configurations and explored their relative performances with different design variations. The performance of VAWTs cluster is significantly affected by several design variables, namely, rotational direction, turbine spacing, farm layout/pattern, wind direction, turbine types, number of turbines, tip speed ratio, pitch control, and wind shear profile. Hence, developing an efficient cluster requires proper modeling and optimization tools, along with high-end experimental tests and prototyping. This paper demonstrates that the wake interaction downstream of VAWTs in a cluster has a positive impact, potentially enhancing the overall performance of the wind farm. However, conversely, the paper also illustrates that the wake interaction has a negative effect on HAWTs farms, leading to a reduction in their overall performance. The computational requirement of VAWTs cluster is very high given the wake interaction between turbines is important in quantifying the farm output. In this regard, CFD-based models, such as LES, RANS, URANS, and DES, and analytical methods, such as the Top-Hat Wake Model, Gaussian Wake Model, Asymmetric Gaussian Wake Model, Actuator Line Model (ALM), Actuator Disk Model (ADM) and Vortex Model are explored. We have found that results from CFD models show more accurate results than the analytical methods. However, the CFD approach necessitates cutting-edge computational resources to model the wake effect, resulting in significant costs associated with running all the simulations. The authors contend that to address the limitations of CFD, the implementation of hybrid models like ALM-LES has proven to be a promising approach for modeling the wake while maintaining the accuracy of the results. In addition to the aforementioned computational efforts, there are few findings on AI and advanced control strategies to enhance the optimization of VAWTs clusters. Finally, the review explored a few case studies done on comparison between the HAWTs and VAWTs clusters, to provide future perspectives and insights based on different comparison criteria such as LCOE, aerodynamic performance, Power density, aerodynamic loads, complexity, Noise, and gain/loss factor. Despite the promising results presented by several researchers, the following research gaps and areas are identified for future exploration to enhance the deployment of VAWTs clusters.

1. Advanced computational models and optimization tools:

- The CFD study has scope for expansion on bigger infrastructure by adding more turbines;
- There is a scarcity of 3D simulations, which should be addressed to enhance the understanding of VAWT clusters;
- To evaluate the impact of atmospheric thermal stability on the performance of co-located wind farms;
- To extend the validation of both computational and analytical wake models to different atmospheric regimes and wind shear characteristics;
- To comprehend different wind-farm layouts such as co-locating, vertical staggered, and other complex cluster configurations;
- To enhance the power generation of co-located wind farms by optimizing the design and placement of clustered VAWTs inside HAWT arrays;
- Coupled and multi-physics modeling, such as FSI, is required to quantify the structural loads due to wake interactions and layout design;
- Application of AI and machine learning to optimize cluster layout; and
- Application of advanced and innovative control strategies such as combined wind farm operation using a predictive model.

2. Refined economic models: To refine the designs for the major components and their cost estimates, to quantify LCOE with reasonable uncertainty for a floating VAWT system. The refinements to the design and cost analysis will include:

- For the rotor inclusion of additional costs such as manufacturing;
- For the platform and mooring, consider additional floater types and re-visit practical design requirements such as free-board height;
- For the drive train, sizing of both direct drive and geared options will be considered along with costing;
- For operations and maintenance costs, including unique VAWT characteristics such as improved drive-train accessibility at the water line;
- For BoS costs for a floating VAWT system, including important costs such as installation, assembly, and electrical infrastructure; and
- To evaluate how a realistic wind rose affects the LCoE computation in co-located wind farms and other configurations

3. Promoting the right technology:

- Developing comprehensive environmental pollution metrics such as noise metrics and psychoacoustic annoyance of the VAWTs vs. HAWTs could clarify the merits of VAWTs;
- Exploring environmental activism and vertical-axis wind turbine preferences in urban areas and offshore locations shall be promoted given their inherent merits and suitability;
- Experimental and prototyping shall foster the application of VAWTs cluster in the wind energy industry;
- In addition to advanced computational approaches, AI could benefit the optimization and enhancement of VAWTs cluster configurations;
- Exploring more optimal VAWTs cluster layouts and co-locating in existing shall enhance VAWTs acceptance in the wind industry; and
- The application of advanced control strategies shall also improve the performance of VAWTs cluster configurations.

Acknowledgement: None.

Funding Statement: The authors received no specific funding for this study.

Author Contributions: The authors confirm contribution to the paper as follows: Study Conception and Design: Ryan Randall, Chunmie Chen, Mesfin Belayneh Ageze, Muluken Temesgen Tigabu; Literature Collection: Mesfin Belayneh Ageze; Draft Manuscript Preparation: Ryan Randall, Mesfin Belayneh Ageze, Muluken Temesgen Tigabu; Final Review and Approval, Manuscript Review and Supervision: Chunmie Chen. All authors reviewed the results and approved the final version of the manuscript.

Availability of Data and Materials: The data presented in this study are available on request from the corresponding author.

Ethics Approval: Not applicable.

Conflicts of Interest: The authors declare no conflicts of interest to report regarding the present study.

References

1. Yolcan OO. World energy outlook and state of renewable energy: 10-year evaluation. *Innov Green Dev.* 2023; 2(4):100070. doi:10.1016/j.igd.2023.100070.
2. Tanürün HE. Improvement of vertical axis wind turbine performance by using the optimized adaptive flap by the Taguchi method. *Energy Sour Part Recov Util Environ Eff.* 2024;46(1):71–90. doi:10.1080/15567036.2023.2279264.
3. Mohammed AA, Ouakad HM, Sahin AZ, Bahaidarah HMS. Vertical axis wind turbine aerodynamics: summary and review of momentum models. *J Energy Resour Technol.* 2019 Feb;141(5):050801. doi:10.1115/1.4042643.
4. Barnes A, Marshall-Cross D, Hughes BR. Towards a standard approach for future Vertical Axis Wind Turbine aerodynamics research and development. *Renew Sustain Energy Rev.* 2021;148(4):111221. doi:10.1016/j.rser.2021.111221.
5. Tigabu MT, Khalid MSU, Wood D, Admasu BT. Some effects of turbine inertia on the starting performance of vertical-axis hydrokinetic turbine. *Ocean Eng.* 2022 May;252(3):111143. doi:10.1016/j.oceaneng.2022.111143.
6. Ghafoorian F, Mirmotahari SR, Eydizadeh M, Mehrpooya M. A systematic investigation on the hybrid Darrieus-Savonius vertical axis wind turbine aerodynamic performance and self-starting capability improvement by installing a curtain. *Energy.* 2025 Jan;6(7):100203. doi:10.1016/j.nxener.2024.100203.
7. Yan D, Yang Y, Ge Z. CFD evaluation of the self-starting of a vertical-axis wave turbine and the related flow and load characteristics. In: *ASME 2024 43rd International Conference on Ocean, Offshore and Arctic Engineering*, 2024 Aug; Singapore: American Society of Mechanical Engineers Digital Collection. doi:10.1115/OMAE2024-125892.
8. Mirmotahari SR, Ghafoorian F, Mehrpooya M, Hosseini Rad S, Taraghi M, Moghimi M. A comprehensive investigation on Darrieus vertical axis wind turbine performance and self-starting capability improvement by implementing a novel semi-directional airfoil guide vane and rotor solidity. *Phys Fluids.* 2024 Jun;36(6):065151. doi:10.1063/5.0208848.
9. Liu K, Yu M, Zhu W. Enhancing wind energy harvesting performance of vertical axis wind turbines with a new hybrid design: a fluid-structure interaction study. *Renew Energy.* 2019;140(4):912–27. doi:10.1016/j.renene.2019.03.120.
10. Wisner KS, Yu M. Vertical-axis turbine performance enhancement with physics-informed blade pitch control. Basic principles and proof of concept with high-fidelity numerical simulation. *J Renew Sustain Energy.* 2024 Mar;16(2):023305. doi:10.1063/5.0178535.
11. Tong M, Zhu W, Zhao X, Yu M, Liu K, Li G. Free and forced vibration analysis of H-type and hybrid vertical-axis wind turbines. *Energies.* 2020;13(24):6747. doi:10.3390/en13246747.
12. Peng HY, Liu HJ, Yang JH. A review on the wake aerodynamics of H-rotor vertical axis wind turbines. *Energy.* 2021;232:121003. doi:10.1016/j.energy.2021.121003.
13. Wang L, Dong M, Yang J, Wang L, Chen S, Duić N, et al. Wind turbine wakes modeling and applications: past, present, and future. *Ocean Eng.* 2024 Oct;309(8):118508. doi:10.1016/j.oceaneng.2024.118508.
14. Watts RG, Ferrer R. The lateral force on a spinning sphere: aerodynamics of a curveball. *Am J Phys.* 1987 Jan; 55(1):40–4. doi:10.1119/1.14969.
15. Sorensen B. *Renewable energy: physics, engineering, environmental impacts, economics and planning.* London: Academic Press; 2017.
16. Kelley CL, Maniaci DC, Resor BR. Horizontal-axis wind turbine wake sensitivity to different blade load distributions. In: *33rd Wind Energy Symposium*, 2015; Kissimmee, FL, USA. doi:10.2514/6.2015-0490.
17. Dabiri JO. Potential order-of-magnitude enhancement of wind farm power density via counter-rotating vertical-axis wind turbine arrays. *J Renew Sustain Energy.* 2011;3(4):043104. doi:10.1063/1.3608170.
18. Lund K, Madsen E. State-of-the-art value chain roadmap for sustainable end-of-life wind turbine blades. *Renew Sustain Energy Rev.* 2024;192:114234.
19. Silva JE, Danao LAM. Varying VAWT cluster configuration and the effect on individual rotor and overall cluster performance. *Energies.* 2021;14(6):1567. doi:10.3390/en14061567.

20. Zheng H-D, Zheng XY, Zhao SX. Arrangement of clustered straight-bladed wind turbines. *Energy*. 2020;200(3):117563. doi:10.1016/j.energy.2020.117563.
21. Mohamed OS, Ibrahim A, El Baz AMR. CFD investigation of the multiple rotors Darrieus type turbine performance. In: *ASME Turbo Expo 2019: Turbomachinery Technical Conference and Exposition*, Jun 17–21, 2019; Phoenix, AZ, USA: American Society of Mechanical Engineers; V009T48A010.
22. Chowdhury AM, Akimoto H, Hara Y. Comparative CFD analysis of vertical axis wind turbine in upright and tilted configuration. *Renew Energy*. 2016;85(1):327–37. doi:10.1016/j.renene.2015.06.037.
23. Ross I, Altman A, Bowman D, Mooney T, Bogart D. Aerodynamics of vertical-axis wind turbines: assessment of accepted wind tunnel blockage practice. In: *48th AIAA Aerospace Sciences Meeting Including the New Horizons Forum and Aerospace Exposition*, 2010; Orlando, FL, USA. doi:10.2514/6.2010-397.
24. Manwell JF, McGowan JG, Rogers AL. *Wind energy explained: theory, design and application*. John Wiley & Sons; 2010.
25. Azadani LN. Vertical axis wind turbines in cluster configurations. *Ocean Eng*. 2023;272(4):113855. doi:10.1016/j.oceaneng.2023.113855.
26. Shaheen M, Abdallah S. Development of efficient vertical axis wind turbine clustered farms. *Renew Sustain Energy Rev*. 2016;63(8):237–44. doi:10.1016/j.rser.2016.05.062.
27. Kinzel M, Mulligan Q, Dabiri JO. Energy exchange in an array of vertical-axis wind turbines. *J Turbul*. 2012;13:N38. doi:10.1080/14685248.2012.712698.
28. Abkar M. Theoretical modeling of vertical-axis wind turbine wakes. *Energies*. 2019;12(1):10. doi:10.3390/en12010010.
29. Lam HF, Peng HY. Measurements of the wake characteristics of co- and counter-rotating twin H-rotor vertical axis wind turbines. *Energy*. 2017;131:13–26. doi:10.1016/j.energy.2017.05.015.
30. Peng HY, Lam HF, Liu HJ. Numerical investigation into the blade and wake aerodynamics of an H-rotor vertical axis wind turbine. *J Renew Sustain Energy*. 2018 Sep;10(5):053305. doi:10.1063/1.5040297.
31. Hand B, Kelly G, Cashman A. Aerodynamic design and performance parameters of a lift-type vertical axis wind turbine: a comprehensive review. *Renew Sustain Energy Rev*. 2021;139(3):110699. doi:10.1016/j.rser.2020.110699.
32. Tjiu W, Marnoto T, Mat S, Ruslan MH, Sopian K. Darrieus vertical axis wind turbine for power generation I: assessment of Darrieus VAWT configurations. *Renew Energy*. 2015;75:50–67. doi:10.1016/j.renene.2014.09.038.
33. Shaheen M, Abdallah S. Efficient clusters and patterned farms for Darrieus wind turbines. *Sustain Energy Technol Assess*. 2017;19(4):125–35. doi:10.1016/j.seta.2017.01.007.
34. Giorgetti S, Pellegrini G, Zanforlin S. CFD Investigation on the aerodynamic interferences between medium-solidity darrieus vertical axis wind turbines. *Energy Proc*. 2015;81:227–39. doi:10.1016/j.egypro.2015.12.089.
35. Whittlesey RW, Liska S, Dabiri JO. Fish schooling as a basis for vertical axis wind turbine farm design*. *Bioinspir Biomim*. 2010 Aug;5(3):035005. doi:10.1088/1748-3182/5/3/035005.
36. Duraisamy K, Lakshminarayan V. Flow physics and performance of vertical axis wind turbine arrays. In: *32nd AIAA Applied Aerodynamics Conference*, 2014; Atlanta, GA, USA: American Institute of Aeronautics; p. 3139.
37. Bremseth J, Duraisamy K. Computational analysis of vertical axis wind turbine arrays. *Theor Comput Fluid Dyn*. 2016;30:387–401.
38. Kinzel M, Araya DB, Dabiri JO. Turbulence in vertical axis wind turbine canopies. *Phys Fluids*. 2015 Nov; 27(11):115102. doi:10.1063/1.4935111.
39. Mereu R, Federici D, Ferrari G, Schito P, Inzoli F. Parametric numerical study of Savonius wind turbine interaction in a linear array. *Renew Energy*. 2017;113(9):1320–32. doi:10.1016/j.renene.2017.06.094.
40. Hezaveh SH, Bou-Zeid E, Dabiri J, Kinzel M, Cortina G, Martinelli L. Increasing the power production of vertical-axis wind-turbine farms using synergistic clustering. *Bound-Layer Meteorol*. 2018;169:275–96.
41. Durkacz J, Islam S, Chan R, Fong E, Gillies H, Karnik A, et al. CFD modelling and prototype testing of a vertical axis wind turbines in planetary cluster formation. *Energy Rep*. 2021;7(2021):119–26. doi:10.1016/j.egy.2021.06.019.

42. Kadum H, Cal RB, Quigley M, Cortina G, Calaf M. Compounded energy gains in collocated wind plants: energy balance quantification and wake morphology description. *Renew Energy*. 2020;150:868–77. doi:10.1016/j.renene.2019.12.077.
43. Chen J, Zhang Y, Xu Z, Li C. Flow characteristics analysis and power comparison for two novel types of vertically staggered wind farms. *Energy*. 2023;263(3):126141. doi:10.1016/j.energy.2022.126141.
44. Belabes B, Paraschivoiu M. CFD modeling of vertical-axis wind turbine wake interaction. *Trans Can Soc Mech Eng*. 2023;47(4):449–58. doi:10.1139/tcsme-2022-0149.
45. Posa A. Wake characterization of coupled configurations of vertical axis wind turbines using large eddy simulation. *Int J Heat Fluid Flow*. 2019;75(4):27–43. doi:10.1016/j.ijheatfluidflow.2018.11.008.
46. Rivera-Arreba I, Li Z, Yang X, Bachynski-Polić EE. Comparison of the dynamic wake meandering model against large eddy simulation for horizontal and vertical steering of wind turbine wakes. *Renew Energy*. 2024 Feb; 221(6):119807. doi:10.1016/j.renene.2023.119807.
47. Ouro P, Lazennec M. Theoretical modelling of the three-dimensional wake of vertical axis turbines. *Flow*. 2021;1: E3. doi:10.1017/flo.2021.4.
48. Yuan Z, Sheng Q, Sun K, Zang J, Zhang X, Jing F, et al. The array optimization of vertical axis wind turbine based on a new asymmetric wake model. *J Mar Sci Eng*. 2021;9(8):820. doi:10.3390/jmse9080820.
49. Dinesh Kumar Reddy G, Verma M, De A. Performance analysis of vertical-axis wind turbine clusters: effect of inter-turbine spacing and turbine rotation. *Phys Fluids*. 2023 Oct;35(10):105122. doi:10.1063/5.0169060.
50. Hezaveh SH, Bou-Zeid E, Lohry MW, Martinelli L. Simulation and wake analysis of a single vertical axis wind turbine. *Wind Energy*. 2017;20(4):713–30. doi:10.1002/we.2056.
51. Rezaeiha A, Montazeri H, Blocken B. On the accuracy of turbulence models for CFD simulations of vertical axis wind turbines. *Energy*. 2019;180(8):838–57. doi:10.1016/j.energy.2019.05.053.
52. Hansen MOL, Sørensen JN, Voutsinas S, Sørensen N, Madsen HA. State of the art in wind turbine aerodynamics and aeroelasticity. *Prog Aerosp Sci*. 2006;42(4):285–330.
53. Oktavitasari D, Kurniawan P, Tjahjana DDDP, Mazlan SA. Study of the wind farm arrangements and wake characteristic using numerical simulation for crossflow wind turbine. *AIP Conf Proc*. 2019 Apr;2097(1): 030009. doi:10.1063/1.5098184.
54. Hansen JT, Mahak M, Tzanakis I. Numerical modelling and optimization of vertical axis wind turbine pairs: a scale up approach. *Renew Energy*. 2021;171(14):1371–81. doi:10.1016/j.renene.2021.03.001.
55. Barnes A, Hughes B. Determining the impact of VAWT farm configurations on power output. *Renew Energy*. 2019;143(5):1111–20. doi:10.1016/j.renene.2019.05.084.
56. Shaheen M. Numerical analysis of the effect of the mutual interaction between closely separated variable pitch vertical axis wind turbines. *Wind Eng*. 2021;45(5):1222–42. doi:10.1177/0309524X20971679.
57. Meziane M, Essadiqi E, Faqir M, Ghanameh MF. CFD study of unsteady flow through Savonius wind turbine clusters. *Int J Renew Energy Res*. 2019;9(2):657–66.
58. Zhang JH, Lien F-S, Yee E. Investigations of vertical-axis wind-turbine group synergy using an actuator line model. *Energies*. 2022;15(17):6211. doi:10.3390/en15176211.
59. Mendoza V, Goude A. Wake flow simulation of a vertical axis wind turbine under the influence of wind shear. *J Phys Conf Ser*. 2017 May;854(1):012031. doi:10.1088/1742-6596/854/1/012031.
60. Shen Z, Gong S, Xie G, Lu H, Guo W. Investigation of the effect of critical structural parameters on the aerodynamic performance of the double darrieus vertical axis wind turbine. *Energy*. 2024 Mar;290:130156. doi:10.1016/j.energy.2023.130156.
61. Kim HH, Oh Y, Yoo HH. Simple vibration model for the design of a vertical axis wind turbine. *J Mech Sci Technol*. 2020;34(2):511–20. doi:10.1007/s12206-020-0101-z.
62. Deng W, Yu Y, Liu L, Guo Y, Zhao H. Research on the dynamical responses of H-type floating VAWT considering the rigid-flexible coupling effect. *J Sound Vib*. 2020;469(6):115162. doi:10.1016/j.jsv.2019.115162.

63. Troldborg N, Larsen GC, Madsen HA, Hansen KS, Sørensen JN, Mikkelsen R. Numerical simulations of wake interaction between two wind turbines at various inflow conditions. *Wind Energy*. 2011;14(7):859–76. doi:10.1002/we.433.
64. Fatahian E, Mishra R, Jackson FF, Fatahian H. Optimization and analysis of self-starting capabilities of vertical axis wind turbine pairs: a CFD-Taguchi approach. *Ocean Eng*. 2024;302(1–3):117614. doi:10.1016/j.oceaneng.2024.117614.
65. Hassanpour M, Azadani LN. Aerodynamic optimization of the configuration of a pair of vertical axis wind turbines. *Energy Convers Manag*. 2021;238(8):114069. doi:10.1016/j.enconman.2021.114069.
66. Chen Y, Chen Y, Zhou J, Guo P, Li J. Optimization and performance study of bidirectional Savonius tidal turbine cluster with deflectors. *Energy Convers Manag*. 2023;283:116947.
67. Ginsbourger D, Le Riche R, Carraro L. Kriging is well-suited to parallelize optimization. In: *Computational intelligence in expensive optimization problems*. Springer; 2010. p. 131–62.
68. Shaaban S, Albatat A, Mohamed MH. Optimization of H-Rotor Darrieus turbines' mutual interaction in staggered arrangements. *Renew Energy*. 2018;125:87–99. doi:10.1016/j.renene.2018.02.094.
69. Lam HF, Peng HY. Development of a wake model for Darrieus-type straight-bladed vertical axis wind turbines and its application to micro-siting problems. *Renew Energy*. 2017;114:830–42. doi:10.1016/j.renene.2017.07.094.
70. Cazzaro D, Bedon G, Pisinger D. Vertical axis wind turbine layout optimization. *Energies*. 2023;16(6):2697. doi:10.3390/en16062697.
71. Hansen M, Enevoldsen P, Abkar M. Energy harvesting via co-locating horizontal-and vertical-axis wind turbines. *J Phys: Conf Ser*. 2020;1618:032004. doi:10.1088/1742-6596/1618/3/032004.
72. Xia G, Cao Y, Qian Z, Zhu Y, Wang J, Guo T, et al. Optimization layout and aerodynamic performance research on double nautilus vertical-axis wind turbine. *Appl Sci*. 2023;13(19):10959. doi:10.3390/app131910959.
73. Chen Y, Guo P, Zhang D, Chai K, Zhao C, Li J. Power improvement of a cluster of three Savonius wind turbines using the variable-speed control method. *Renew Energy*. 2022;193(2012):832–42. doi:10.1016/j.renene.2022.05.062.
74. Weihs D. Some hydrodynamical aspects of fish schooling. *Swim Fly Nat*. 1975;2:703–18. doi:10.1007/978-1-4757-1326-8.
75. Chen H. Cluster-based ensemble learning for wind power modeling from meteorological wind data. *Renew Sustain Energy Rev*. 2022;167(5):112652. doi:10.1016/j.rser.2022.112652.
76. Zhang J, Zhao X. Digital twin of wind farms via physics-informed deep learning. *Energy Convers Manag*. 2023;293:117507.
77. Li R, Zhang J, Zhao X. Dynamic wind farm wake modeling based on a Bilateral Convolutional Neural Network and high-fidelity LES data. *Energy*. 2022;258(8):124845. doi:10.1016/j.energy.2022.124845.
78. Udo WS, Kwakye JM, Ekechukwu DE, Ogundipe OB. Optimizing wind energy systems using machine learning for predictive maintenance and efficiency enhancement. *J Renew Energy Technol*. 2024;28(3):312–30.
79. Fadil J, Soedibyo S, Ashari M. Novel of vertical axis wind turbine with variable swept area using fuzzy logic controller. *Int J Intell Eng Syst*. 2020;13(3):256–67. doi:10.22266/ijies2020.0630.24.
80. Brandetti L, Mulders SP, Merino-Martinez R, Watson S, van Wingerden J-W. Multi-objective calibration of vertical-axis wind turbine controllers: balancing aero-servo-elastic performance and noise. *Wind Energy Sci Discuss*. 2023;2023:1–34.
81. Aboezz A, Ghali H, Elbayomi G, Madboli M. A novel VAWT passive flow control numerical and experimental investigations: guided vane airfoil wind turbine. *Ocean Eng*. 2022;257(1):111704. doi:10.1016/j.oceaneng.2022.111704.
82. Xu W, Li G, Wang F, Li Y. High-resolution numerical investigation into the effects of winglet on the aerodynamic performance for a three-dimensional vertical axis wind turbine. *Energy Convers Manag*. 2020;205:112333.
83. Abbasi S, Daraee MA. Improving vertical-axis wind turbine performance through innovative combination of deflector and plasma actuator. *Phys Fluids*. 2024 Apr;36(4):045134. doi:10.1063/5.0204070.

84. Xu Z, Chen J, Li C. Research on the adaptability of dynamic pitch control strategies on H-type VAWT close-range arrays by simulation study. *Renew Energy*. 2023;218(4):119231. doi:10.1016/j.renene.2023.119231.
85. Howland MF, Quesada JB, Martínez JP, Larrañaga FP, Yadav N, Chawla JS, et al. Collective wind farm operation based on a predictive model increases utility-scale energy production. *Nat Energy*. 2022;7(9):818–27. doi:10.1038/s41560-022-01085-8.
86. Zhang L, Feng Z, Zhao Y, Xu X, Feng J, Ren H, et al. Experimental study of wake evolution under vertical staggered arrangement of wind turbines of different sizes. *J Mar Sci Eng*. 2024 Mar;12(3):3. doi:10.3390/jmse12030434.
87. Vergaerde A, Troyer TD, Muggiasca S, Bayati I, Belloli M, Kluczevska-Bordier J, et al. Experimental characterisation of the wake behind paired vertical-axis wind turbines. *J Wind Eng Ind Aerodyn*. 2020;206(4):104353. doi:10.1016/j.jweia.2020.104353.
88. Huang M, Vijaykumar Patil Y, Sciacchitano A, Ferreira C. Experimental study of the wake interaction between two vertical axis wind turbines. *Wind Energy*. 2023;26(11):1188–211. doi:10.1002/we.2863.
89. Su H, Meng H, Qu T, Lei L. Wind tunnel experiment on the influence of array configuration on the power performance of vertical axis wind turbines. *Energy Convers Manag*. 2021;241:114299. doi:10.1016/j.enconman.2021.114299.
90. Shelley SA, Boo SY, Kim D, Luyties WH. Comparing levelized cost of energy for a 200 MW floating wind farm using vertical and horizontal axis turbines in the Northeast U.S.A. In: *OTC Offshore Technology Conference*, 2018; Houston, TX, USA. doi:10.4043/28700-MS.
91. Shields M, Beiter P, Kleiber W. Spatial impacts of technological innovations on the levelized cost of energy for offshore wind power plants in the United States. *Sustain Energy Technol Assess*. 2021;45(17):101059. doi:10.1016/j.seta.2021.101059.
92. Beiter P, Musial W, Kilcher L, Sirmivas S, Stehly T, Gevorgian V, et al. A spatial-economic cost-reduction pathway analysis for U.S. In: *Offshore wind energy development from 2015–2030*. USA: National Renewable Energy Lab; 2016. Available from: <https://api.semanticscholar.org/CorpusID:114164082>. [Accessed 2024].
93. Viqueira-Moreira M, Ferrer E. Insights into the aeroacoustic noise generation for vertical axis turbines in close proximity. *Energies*. 2020;13(16):4148. doi:10.3390/en13164148.
94. Todd Griffith D, Paquette J, Barone M, Goupee AJ, Fowler MJ, Bull D, et al. A study of rotor and platform design trade-offs for large-scale floating vertical axis wind turbines. *J Phys: Conf Ser*. 2016;753:102003. doi:10.1088/1742-6596/753/10/102003.
95. Vranešević KK, Ćorić S, Glumac AŠ. LES study on the urban wind energy resources above the roof of buildings in generic cluster arrangements: impact of building position. *J Wind Eng Ind Aerodyn*. 2023;240(1):105503. doi:10.1016/j.jweia.2023.105503.
96. Kwok KCS, Hu G. Wind energy system for buildings in an urban environment. *J Wind Eng Ind Aerodyn*. 2023;234:105349. doi:10.1016/j.jweia.2023.105349.
97. Li S, Lu W-T, Phillips BM, Jiang Z. Flow characteristics over flat building roof with different edge configurations for wind energy harvesting: a wind tunnel study. *Energy Build*. 2024 Nov;323(7282):114789. doi:10.1016/j.enbuild.2024.114789.
98. Paraschivoiu I, Ammar S, Saeed F. VAWT versus HAWT: a comparative performance study of 2–6 MW rated capacity turbines. *Eng Can Soc Mech Eng*. 2018;42(4):393–403. doi:10.1139/tcsme-2017-0137.
99. Möllerström E, Ottermo F, Hylander J, Bernhoff H. Noise emission of a 200 kW vertical axis wind turbine. *Energies*. 2016;9(1):19. doi:10.3390/en9010019.
100. Xie S, Archer CL, Ghaisas N, Meneveau C. Benefits of collocating vertical-axis and horizontal-axis wind turbines in large wind farms. *Wind Energy*. 2017;20(1):45–62. doi:10.1002/we.1990.