

Synthetic iterative scheme for thermal applications in hotspot systems with large temperature variance

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Abstract

A synthetic iterative scheme is developed for thermal applications in hotspot systems with large temperature variance. Different from previous work with linearized equilibrium state and small temperature difference assumption, the phonon equilibrium distribution shows a nonlinear relationship with temperature and mean free path changes with the spatial temperature when the temperature difference of system is large, so that the same phonon mode may suffer different transport processes in different geometric regions. In order to efficiently capture nonlinear and multiscale thermal behaviors, the Newton method is used and a macroscopic iteration is introduced for preprocessing based on the iterative solutions of the stationary phonon BTE. Macroscopic and mesoscopic physical evolution processes are connected by the heat flux, which is no longer calculated by classical Fourier's law but obtained by taking the moment of phonon distribution function. These two processes exchange information from different scales, such that the present scheme could efficiently deal with heat conduction problems from ballistic to diffusive regime. Numerical tests show that the present scheme could efficiently capture the multiscale heat conduction in hotspot systems with large temperature variances. In addition, a comparison is made between the solutions of the present scheme and effective Fourier's law by several heat dissipations problems under different sizes or selective phonon excitation. Numerical results show that compared to the classical Fourier's law, the results of the effective Fourier's law could be closer to the BTE solutions by adjusting effective coefficients. However, it is still difficult to capture some local nonlinear phenomena in complex geometries.

Keywords: Micro/nano scale heat conduction, Boltzmann transport equation, Synthetic iterative scheme, Effective Fourier's law, Hotspot issue, Transistors

1. INTRODUCTION

With the continuous development of modern semiconductor process technology, the characteristic size of electronic devices decreases sharply from microns to nanometers and the hotspot issues become increasingly

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serious, which have attracted great attention in academic [1, 2, 3] and industrial [4, 5, 6] communities. Micro/nano scale thermal management in hotspot systems is particularly important because it will seriously reduce working efficiency and device life, but it faces huge challenge [2]. Firstly, the heat generation in electronic devices mainly results from the interaction between electrons and phonons when the electric field drives the electrons to migrate from the source to the drain [7, 8, 9]. The energy weights obtained by different phonon modes from electrons in this process are non-uniform, namely, this is a selective phonon excitation or non-thermal heating process [10, 11, 9]. Secondly, when the system size is comparable to or smaller than phonon mean free path, ballistic phonon transport plays an important role on heat conduction [12, 11]. Many experimental studies in the past 30 years have proven that the classical Fourier’s law with bulk thermal conductivity cannot well predict the thermal behaviors in the solid materials at the micro/nano scales [13, 14, 15, 16, 17, 18, 19, 20].

In order to efficiently solve the practical multiscale heat conduction problems, many models have been developed [21, 22, 23, 24]. One of the most commonly used and simplest models is a combination of the macroscopic equations and effective empirical coefficients. For example, the effective Fourier’s law,

$$\mathbf{q} = -\kappa_{eff}(\mathbf{x}, T)\nabla T, \quad (1)$$

is widely used in the practical multiscale thermal application [25, 26, 27] and the post-processing of most micro/nano scale thermal experiments [17, 18], where a size- (or spatial) and temperature- dependent effective thermal conductivity is introduced instead of the bulk thermal conductivity. Different effective thermal conductivity coefficients are used for different materials with various sizes, and external heat sources in the macroscopic equations usually default to uniformly heating all (quasi)particles. The effective Fourier’s law has been integrated into major commercial softwares, such as ANSYS, TCAD and COMSOL, and applied to multi-physics coupling simulations in actual 3D electronic devices (e.g., fin or gate-all-around field-effect transistors, FinFETs/GAAFETs) [25, 26, 27, 28, 6], where the choice of effective thermal conductivity is somewhat related to the experience of the engineers. Until today, there are few in-depth studies of how far the predictions of the effective Fourier’s law deviate from the mesoscopic models or experiments at the micro/nano scale [13].

Another popular model is the mesoscopic Boltzmann transport equation (BTE), which ignores coherence but can still give reasonable predictions and capture some physical insights such as the self-heating [29, 30, 26, 27], ballistic effects [31] and selective phonon excitations [11, 9]. The self-heating and ballistic effects in transistors are widely studied under the framework of phonon BTE by many scientific research institutions [7, 32], such as IMEC [6] and Intel [5]. NanoHeat group led by Prof. Kenneth E. Goodson has made excellent progress on this topic in the past 30 years [33]. They calculated detailed electron-phonon coupling processes, simulated self-heating effects and small scale heat dissipations in transistors [7, 34]. In addition, some researchers have paid attention to the effects of selective phonon excitation on micro/nano scale heat conduction in semi-conductor materials [10, 11, 9]. Under the framework of phonon BTE, Chiloyan

and Huberman *et al.* [11] found that selective phonon excitation in silicon materials can lead to enhanced heat conduction beyond Fourier’s predictions by targeted heating particular phonon modes, for example, only heating phonon modes with larger mean free path. Huberman and Zhang *et al.* [35] found that in quasi-1D frequency-domain thermoreflectance geometry the relationship between heating-frequency and phase lag in germanium materials is different under various selective phonon excitation. Xu *et al.* [9] found that the peak temperature rise in a silicon quasi-2D bulk FinFET is much larger than that predicted by classical Fourier’s law if the non-equilibrium or selective phonon excitation effect is ignored.

Actually it is hard to obtain the analytical solutions of phonon BTE in practical thermal applications so that many numerical methods are developed for simulating micro/nano scale heat conduction problems [23, 36, 37]. One of the most popular methods is the ensemble Monte Carlo method, which uses statistical particles to represent the actual transport or scattering processes [38, 39, 40]. It has been widely used for simulating the practical heat dissipations in three-dimensional transistors [41, 42, 43]. However, its time step and cell size have to be smaller than the relaxation time and mean free path due to the separate treatment of advection and scattering in single time step. In addition, the statistics errors and computational cost of Monte Carlo method (regardless of ensemble, steady-state or low-variance) increase rapidly [44, 45, 46, 47] when system size increases significantly, so that it is very hard for Monte Carlo method to efficiently predict the thermal distributions in the (near) diffusive regime. In order to reduce computational cost, the hybrid method is used [37] whose basic idea is to discretize the whole computational domain into two or several parts. The phonon BTE is solved in some domains where ballistic phonon transport dominates, and effective Fourier’s law is used in other areas. This method has also been applied successfully in the heat dissipations of electronic devices. However, reasonable domain decomposition is very empirical and influences the final results significantly. Another numerical method is to directly solve phonon BTE by discretizing the seven-dimensional phase space into a lot of small pieces [48, 9], which has no statistics errors but requires a huge number of computational memories, for example discrete ordinate method (DOM). It adopts iterative strategies to solve the phonon BTE in the whole spatial space for a given point in wave vector space. And then repeat the whole wave vector space to update the macroscopic distributions at the next step. One of the main drawback of this method is the slow convergence speed in the (near) diffusive regime [49, 50, 51].

In order to solve the drawback of DOM, we have proposed a synthetic iterative scheme to efficiently solve the stationary phonon BTE since 2017 [50, 52, 53, 51], which accelerates convergence significantly compared to DOM in the (near) diffusive regime. It has also been made into an open source package GiftBTE by Prof Hua Bao’s group [54] and applied for the heat dissipations in transistors [55]. However, previous synthetic iterative scheme usually used a linearized equilibrium state with small temperature difference assumptions, which may not be suitable for the practical heat dissipations in real transistors due to large temperature rise. When the temperature difference in the whole domain is large, many thermal parameters including the phonon mean free path, scattering rates and thermal conductivity change with spatial position, which

increases the nonlinear and multiscale characteristics of phonon transport. Hence, it is very necessary to consider the temperature-dependent effects [56] for practical thermal applications [28, 5].

In this work, a synthetic iterative scheme is developed for thermal applications with large temperature variance. Numerical tests show that the present scheme could efficiently capture the multcale heat conduction in hotspot systems with large temperature variances. In addition, the heat dissipations in hotspot systems with a variety of geometric structures, selective phonon excitation and sizes are simulated to estimate the deviations between the effective Fourier's law and phonon BTE. The rest of this article is organized as follows. Phonon BTE and synthetic iterative scheme for large temperature variance are introduced in Section 2 and Section 3, respectively. Numerical tests and discussions are conducted in Section 4. In Section 5, a comparison is made between the solutions of phonon BTE and effective Fourier's law. Finally, a conclusion is made in Section 6.

2. Phonon Boltzmann transport equation

To capture the non-Fourier heat conduction in hotspot systems, the stationary phonon Boltzmann transport equation (BTE) under the relaxation time approximation is used [8, 9, 11, 6, 53]

$$\mathbf{v}_k \cdot \nabla_{\mathbf{x}} g_k = \frac{g_k^{eq} - g_k}{\tau_k} + p_k \dot{S}, \quad (2)$$

where g_k is the distribution function of energy density for phonon mode k (defined by a phonon branch and wave vector in the first Brillouin zone), \mathbf{x} is the spatial position, \mathbf{v}_k is the phonon group velocity obtained by phonon dispersion and $\tau_k = \tau_k(T)$ is the temperature-dependent relaxation time which will be discussed later. g_k^{eq} is the equilibrium state, equal to the Bose-Einstein distribution multiplied by the energy $\hbar\omega$ possessed by each phonon mode [8],

$$g_k^{eq} = \hbar\omega \frac{1}{\exp\left(\frac{\hbar\omega}{k_B T}\right) - 1}, \quad (3)$$

where \hbar is the Planck constant reduced by 2π , ω is the angular frequency and k_B is the Boltzmann constant. \dot{S} is the external heat source or heat generating power density at the macroscopic level, and p_k is associated weight of energy absorbed by each phonon mode from the external heat source satisfying

$$\int p_k d\mathbf{K} = 1, \quad (4)$$

where $d\mathbf{K}$ represents an integral over the whole wave vector space and phonon branches. Although it was usually assumed that the heat source energy is allocated to all phonon modes according to thermal equilibrium in macroscopic thermal simulations or most of previous non-Fourier thermal analysis based on phonon BTE, selective phonon excitation is widespread in thermal management of microelectronics [7, 11, 9, 29].

The local energy density U and heat flux \mathbf{q} could be updated by taking the moment of phonon distribution functions,

$$U = \int g_k d\mathbf{K}, \quad (5)$$

$$\mathbf{q} = \int \mathbf{v}_k g_k d\mathbf{K}. \quad (6)$$

The temperature cannot be well defined in non-equilibrium system. In order to deal with such non-equilibrium systems, the concept of local thermal equilibrium is introduced, namely, there is a local equilibrium at which the energy density obtained by taking moment of the phonon equilibrium distribution with local equivalent equilibrium temperature T is the same as that obtained by taking moment of the non-equilibrium phonon distribution [8],

$$\int g_k^{eq}(T) d\mathbf{K} = \int g_k d\mathbf{K}. \quad (7)$$

A pseudo-temperature T_p is introduced to ensure the energy conservation of the phonon scattering term [38],

$$\int \frac{g_k^{eq}(T_p) - g_k}{\tau_k(T)} d\mathbf{K} = 0. \quad (8)$$

When τ_k is a constant, $T_p = T$.

We mainly simulated the heat conduction in monocrystalline silicon [5, 41, 54] and phonon dispersion in the [1 0 0] direction is chosen to represent the other directions. Dispersion curves of one longitudinal acoustic/optical phonon branch (LA/LO) and two degenerate transverse acoustic/optical phonon branches (TA/TO) are approximated by empirical quadratic polynomial dispersions, as shown in Table. 1 [7], where $\omega = c_0 + c_1 k + c_2 k^2$ and k is the wave vector in [1 0 0] direction. Under the isotropic wave vector space assumption, we have $\mathbf{v}_k = v_g \mathbf{s}$, where $v_g = \partial\omega/\partial k = c_1 + 2c_2 k$, $\mathbf{s} = (\cos \theta, \sin \theta \cos \varphi, \sin \theta \sin \varphi)$ is the unit directional vector with polar angle $\theta \in [0, \pi]$ and azimuthal angle $\varphi \in [0, 2\pi]$. Optical phonons have much small group velocity and contribute a little to the thermal conduction in silicon so that they are usually ignored in some previous studies [39, 40, 53]. Based on a previous paper of heat dissipations in transistor [32], an average value of relaxation time for longitudinal/transverse optical phonon is used in this work, i.e., 3.5 ps. Matthiessen's rule is used to coupled various scattering mechanisms of acoustic phonon together including the impurity scattering, umklapp (U) and normal (N) phonon-phonon scattering,

$$\tau^{-1} = \tau_{\text{impurity}}^{-1} + \tau_{\text{U}}^{-1} + \tau_{\text{N}}^{-1} = \tau_{\text{impurity}}^{-1} + \tau_{\text{NU}}^{-1}, \quad (9)$$

as shown in Table. 2.

3. Synthetic iterative scheme with large temperature variance

To solve the phonon BTE iteratively, a semi-implicit scheme is firstly introduced,

$$\mathbf{v}_k \cdot \nabla g_k^{n+1/2} = \frac{g_k^{eq}(T_p^n) - g_k^{n+1/2}}{\tau_k(T^n)} + p_k \dot{S}^n, \quad (10)$$

Table 1: Quadratic phonon dispersion coefficients of monocrystalline silicon [7], where $\omega = c_0 + c_1k + c_2k^2$ and k is the wave vector in [1 0 0] direction.

Branch	c_0 (10^{13} rad/s)	c_1 (10^5 cm/s)	c_2 (10^{-3} cm ² /s)
LA	0	9.01	-2.0
TA	0	5.23	-2.26
LO	9.88	0	-1.60
TO	10.20	-2.57	1.11

Table 2: Phonon scattering rates of monocrystalline silicon [48], where $a = 0.543$ nm is the lattice constant of silicon.

$\tau_{\text{impurity}}^{-1}$	$A_i\omega^4$, $A_i = 1.498 \times 10^{-45}$ s ³ ;
LA	$\tau_{\text{NU}}^{-1} = B_L\omega^2T^3$, $B_L = 1.180 \times 10^{-24}$ K ⁻³ ;
	$\tau_{\text{NU}}^{-1} = B_T\omega T^4$, $0 \leq k < \pi/a$;
TA	$\tau_{\text{NU}}^{-1} = B_U\omega^2/\sinh(\hbar\omega/k_B T)$, $\pi/a \leq k \leq 2\pi/a$;
	$B_T = 8.708 \times 10^{-13}$ K ⁻³ , $B_U = 2.890 \times 10^{-18}$ s.

where the equilibrium state $g_k^{eq}(T_p^n)$ is at the n -th iteration step and the distribution function is at the $n + 1/2$ -th iteration step $g_k^{n+1/2}$. Make a transformation of Eq. (10),

$$\frac{\Delta g_k^n}{\tau_k^n} + \mathbf{v}_k \cdot \nabla (\Delta g_k^n) = \frac{g_k^{eq}(T_p^n) - g_k^n}{\tau_k(T^n)} + p_k \dot{S}^n - \mathbf{v}_k \cdot \nabla g_k^n, \quad (11)$$

where $\Delta g^n = g^{n+1/2} - g^n$. For a given phonon mode k , the finite volume method is used to discretize the whole spatial space and the Gauss' flux theorem is used to deal with the spatial divergence, then Eqs. (10,11) become following two equations, respectively,

$$\frac{1}{V_i} \sum_{j \in N(i)} S_{ij} \mathbf{n}_{ij} \cdot \mathbf{v}_k g_{ij,k}^{n+1/2} = \frac{g_{i,k}^{eq}(T_p^n) - g_{i,k}^{n+1/2}}{\tau_k(T_i^n)} + p_k \dot{S}_i^n, \quad (12)$$

$$\frac{\Delta g_{i,k}^n}{\tau_k(T_i^n)} + \frac{1}{V_i} \sum_{j \in N(i)} S_{ij} \mathbf{n}_{ij} \cdot \mathbf{v}_k \Delta g_{ij,k}^n = \frac{g_{i,k}^{eq}(T_p^n) - g_{i,k}^n}{\tau_k(T_i^n)} + p_k \dot{S}_i^n - \frac{1}{V_i} \sum_{j \in N(i)} S_{ij} \mathbf{n}_{ij} \cdot \mathbf{v}_k g_{ij,k}^n, \quad (13)$$

where V_i is the volume of the spatial cell i , $N(i)$ is the sets of face neighbor cells of cell i , ij is the interface between the cell i and cell j , S_{ij} is the area of the interface ij , and \mathbf{n}_{ij} is the normal of the interface ij directing from the cell i to the cell j . $g_{i,k}^{n+1/2}$ (or $g_{ij,k}^{n+1/2}$) is the phonon distribution function at discretized spatial cell i (or cell interface ij). It is found that the final numerical accuracy is totally controlled by the right-hand side of Eq. (13) since at steady state $\Delta g \rightarrow 0$. Hence, the reconstruction of the distribution function $g_{ij,k}^n$ at the cell interface determines the spatial accuracy of the present scheme.

In other words, the left hand side of Eq. (13) does not affect the final convergent solutions, so that a simple first-order upwind scheme is used to deal with $\Delta g_{ij,k}^n$

$$\Delta g_{ij,k} = \begin{cases} \Delta g_{i,k}, & \mathbf{n}_{ij} \cdot \mathbf{v}_k \geq 0 \\ \Delta g_{j,k}, & \mathbf{n}_{ij} \cdot \mathbf{v}_k < 0 \end{cases} \quad (14)$$

First-order upwind scheme is numerically stable and efficient in the ballistic regime, but has poor spatial accuracy in the (near) diffusive regime, so that we need to use a higher-order numerical scheme to deal with the right hand side of Eq. (13) in order to improve the final spatial accuracy in the (near) diffusive regime. The phonon BTE is solved again at the cell interface along the group velocity direction with a certain length $|\mathbf{v}_k \Delta t|$,

$$\mathbf{v}_k \frac{g_k^n(\mathbf{x}_{ij}) - g_k^n(\mathbf{x}_{ij} - \mathbf{v}_k \Delta t)}{\mathbf{v}_k \Delta t} = \frac{g_k^{eq}(T_{p,ij}^n) - g_k^n(\mathbf{x}_{ij})}{\tau_k(T_{ij}^n)} + p_k \dot{S}_{ij}^n, \quad (15)$$

$$\implies g_k^n(\mathbf{x}_{ij}) = \frac{\tau_k g_k^n(\mathbf{x}_{ij} - \mathbf{v}_k \Delta t) + \Delta t g_k^{eq}(T_{p,ij}^n) + \tau_k \Delta t p_k \dot{S}_{ij}^n}{\Delta t + \tau_k(T_{ij}^n)}, \quad (16)$$

where $g_k^n(\mathbf{x}_{ij} - \mathbf{v}_k \Delta t)$ or $T_{p,ij}^n$, T_{ij}^n is obtained by the numerical interpolation of macroscopic or mesoscopic distributions at the cell center, i.e., $g_k^n(\mathbf{x}_i)$ or $T_{p,i}^n$, T_i^n . Take quasi-1D as an example, i.e.,

$$T_{ij}^n = \frac{|\mathbf{x}_j - \mathbf{x}_{ij}|}{|\mathbf{x}_j - \mathbf{x}_i|} T_i^n + \frac{|\mathbf{x}_i - \mathbf{x}_{ij}|}{|\mathbf{x}_j - \mathbf{x}_i|} T_j^n, \quad (17)$$

$$T_{p,ij}^n = \frac{|\mathbf{x}_j - \mathbf{x}_{ij}|}{|\mathbf{x}_j - \mathbf{x}_i|} T_{p,i}^n + \frac{|\mathbf{x}_i - \mathbf{x}_{ij}|}{|\mathbf{x}_j - \mathbf{x}_i|} T_{p,j}^n, \quad (18)$$

$$g_k^n(\mathbf{x}_{ij} - \mathbf{v}_k \Delta t) = \begin{cases} g_k^n(\mathbf{x}_i) + \boldsymbol{\sigma}_{i,k} \cdot (\mathbf{x}_{ij} - \mathbf{x}_i - \mathbf{v}_k \Delta t), & \mathbf{v}_k \cdot \mathbf{n}_{ij} > 0, \\ g_k^n(\mathbf{x}_j) + \boldsymbol{\sigma}_{j,k} \cdot (\mathbf{x}_{ij} - \mathbf{x}_j - \mathbf{v}_k \Delta t), & \mathbf{v}_k \cdot \mathbf{n}_{ij} < 0. \end{cases} \quad (19)$$

where van Leer limiter is used for the spatial gradients $\boldsymbol{\sigma}$ of phonon distribution function, i.e.,

$$\begin{cases} s_1 = \frac{g_k(\mathbf{x}_i) - g_k(\mathbf{x}_{i+1})}{\mathbf{x}_i - \mathbf{x}_{i+1}}, & s_2 = \frac{g_k(\mathbf{x}_i) - g_k(\mathbf{x}_{i-1})}{\mathbf{x}_i - \mathbf{x}_{i-1}}, \\ \boldsymbol{\sigma}_{i,k} = (\text{sgn}(s_1) + \text{sgn}(s_2)) \frac{|s_1| |s_2|}{|s_1| + |s_2|}. \end{cases} \quad (20)$$

Δt is a time step and satisfies

$$\Delta t = c_1 \times \frac{\Delta x_{min}}{2v_{max}}, \quad (21)$$

where Δx_{min} is the minimum discretized cell size, v_{max} is the maximum group velocity, c_1 is a dimensionless parameter. In the present simulations, $c_1 = 0.95$. Combining Eqs. (14,13,16), the phonon distribution function $g_{i,k}^{n+1/2}$ or $g_{ij,k}^{n+1/2}$ can both be calculated. More details can be found in our previous paper [51].

Repeat the above process and traverse all phonon modes, then the phonon distribution functions $g_k^{n+1/2}$ in the whole phase space can be obtained. The macroscopic pseudo-temperature at the $n + 1/2$ -th iteration step and temperature at the next iteration step are updated based on Eqs. (8,7),

$$\sum w_k \left(\frac{g_k^{eq}(T_p^{n+1/2}) - g_k^{n+1/2}}{\tau_k(T^n)} \right) = 0, \quad (22)$$

$$\sum w_k \left(g_k^{n+1/2} - g_k^{eq}(T^{n+1}) \right) = 0, \quad (23)$$

where w_k is the associated weight of numerical quadrature \sum over the first Brillouin zone and all phonon branches. Above two nonlinear equations are solved iteratively by Newton method [56] to update the

(pseudo)temperature. If setting $T_p^{n+1} = T_p^{n+1/2}$, then it is the typical implicit DOM which converges fast in the ballistic regime but converges much slowly in the (near) diffusive regime [50].

Secondly, a macroscopic iteration is introduced to accelerate convergence in the (near) diffusive regime. Considering first law of the thermodynamics at steady state,

$$\nabla \cdot \mathbf{q} = \dot{S}, \quad (24)$$

then a macroscopic residual is defined as

$$\text{RES} = -\nabla \cdot \mathbf{q} + \dot{S} = -Q(T, T_p), \quad (25)$$

where $Q(T, T_p)$ is a functional to represent the real relationship between the heat flux and temperature. Eq. (25) is valid from the ballistic to diffusive regime. Note that the real relationship Q between the heat flux and temperature are unknown so that the inexact Newton method [57] is used to solve it iteratively. More details can be found in our previous paper [50]. An approximated linear operator \tilde{Q} is introduced to find an increment of pseudo-temperature ΔT_p for diminishing the macroscopic residual so that a macroscopic iteration can be constructed,

$$\tilde{Q}(T_p^{n+1}) - \tilde{Q}(T_p^{n+1/2}) = \text{RES}^{n+1/2} \quad (26)$$

$$\tilde{Q}(\Delta T_p^{n+1/2}) = \text{RES}^{n+1/2}, \quad (27)$$

where

$$\Delta T_p^{n+1/2} = T_p^{n+1} - T_p^{n+1/2}. \quad (28)$$

Equation (24) is satisfied when the macroscopic residual vanishes, and the approximated linear operator does not affect the final convergent solutions based on the theorem of inexact Newton method [57, 50]. Theoretically the convergence speed is faster if the approximated linear operator is closer to the real operator [57, 50], so that an effective Fourier's law is used for the linear operator,

$$\tilde{Q}(\Delta T_p) = \nabla \cdot (-\beta \cdot \nabla(\Delta T_p)), \quad (29)$$

where β is the same dimension as thermal conductivity. In this paper β is a constant for simplicity, equal to the bulk thermal conductivity κ_{bulk} at the initial ambient temperature. Theoretically, we can implement more detailed treatments of β to reach a faster convergence speed based on the theorem of inexact Newton method.

Similarly finite volume method is used for the discretization of Eq. (27),

$$-\sum_{j \in N(i)} S_{ij} \mathbf{n}_{ij} \cdot \left(\kappa_{\text{bulk}} \cdot \nabla(\Delta T_{p,ij}^{n+1/2}) \right) = \text{RES}_i^{n+1/2} = -\sum_{j \in N(i)} S_{ij} \mathbf{n}_{ij} \cdot \mathbf{q}_{ij}^{n+1/2} + \dot{S}_i^n, \quad (30)$$

where

$$\mathbf{q}_{ij}^{n+1/2} = \sum w_k \mathbf{v}_k g_{ij,k}^{n+1/2}. \quad (31)$$

Conjugate gradient method is used to solve the above diffusion equation (30). The heat flux in the macroscopic equation (30) is obtained by taking the moment of phonon distribution function, rather than the classical or effective Fourier’s law. The heat flux obtained by this strategy is valid from ballistic to diffusive regime. Macroscopic and mesoscopic iterative processes exchange information from different scales, such that the present scheme could efficiently deal with heat conduction problems from ballistic to diffusive regime. The final convergent solutions are totally controlled by the phonon BTE, and the macroscopic operator only plays an accelerate role. Compared to the iterative solutions of the phonon BTE, the computational cost of the macroscopic iteration is very small due to the less degree of freedom. For details of isothermal or diffusely/specular reflecting adiabatic boundary conditions, please see our previous paper [51]. [The present work mainly focus on the steady problem by numerically solving the phonon BTE with infinite time step. What we need to do is to use a finite physical time step to replace the infinite time step in Eq. \(10\) or \(11\) if we want to extend the present scheme for unsteady problem, which is named as dual time-stepping implicit strategy in the computational fluid dynamics areas \[58\].](#)

At the end of this section, let’s briefly analyze, why the above discrete method is used and why this treatment can accelerate convergence from a physical point of view. [A relatively more rigorous numerical analysis of the present scheme in the diffusive limit is also conducted in Appendix A.](#) Steady-state phonon BTE mainly describes the evolution of phonon distribution function in the spatial space and wave vector space. Different phonon modes migrate freely or scatter with other phonons in six-dimensional phase space, and the average distance between two adjacent phonons scattering is the phonon mean free path. For the mesoscopic iteration (10), it assumes that the macroscopic distributions or equilibrium states are fixed for a given phonon mode, and then updates the phonon distribution function in the whole spatial space. In other words, it is assumed that phonons do not interact with other phonon modes and the corresponding equilibrium states remain unchanged when the phonon distribution function is updated and evolved in the spatial space. When all phonon distribution functions are updated, then the macroscopic distributions or equilibrium states are updated based on the conservation principle of phonon scattering (23,22). This method decouples phonon migration from scattering in one iteration step, which indicates that it efficiently updates the distribution function in the spatial space within the range of a mean free path in one iteration step. In the ballistic regime, phonon scattering is rare and the phonon mean free path is comparable to or larger than system size. This method is in good agreement with the actual physical evolution process, so the convergence speed is fast. However, in the (near) diffusive regime, phonon scattering is much frequent and the phonon mean free path is much smaller than system size, so that it converges very slowly.

In order to accelerate convergence in the (near) diffusive regime, we need to make the numerical treatments follow the actual laws of physical evolution [50, 52, 53, 51, 49]. Note that first law of thermodynamics is valid at any scales, which contains an unknown relationship between the heat flux and temperature. Fortunately, this relationship is close to effective/classical Fourier’s law and temperature propagation follows the law of

diffusion in the (near) diffusive regime. Furthermore, both the heat flux (6) and temperature (7,8) could be obtained by taking the moment of distribution function under the framework of BTE from the ballistic to diffusive regime. In other words, this complex relationship between (pseudo-)temperature and heat flux could be explicitly constructed by the mesoscopic distribution function. In the (near) diffusive regime, although the convergence speed of mesoscopic iteration is very slow, it correctly gives a phonon distribution function in the spatial space within the range of a mean free path, from which the corresponding heat flux distribution (31) or macroscopic residual (27) can be obtained. Then a macroscopic iteration can be invoked on the basis of the mesoscopic iteration and connected by the heat flux, which is calculated by taking the moment of phonon distribution function. The drawback of mesoscopic iteration in the (near) diffusive regime is compensated by the macroscopic iteration, by introducing an approximate Fourier operator to achieve fast convergence based on the theorem of inexact Newton method [50]. The unknown relationship between the heat flux and temperature in the macroscopic iteration is compensated by the mesoscopic iteration.

4. Results and discussions

Without special statements, the isotropic wave vector space is divided into N_B equal parts using the rectangular integration rule along the radial direction from 0 to $2\pi/a$ for each phonon branch, where $a = 0.543$ nm is the lattice constant of silicon. The solid angle space is discretized into $N_{dir} = N_\theta \times N_\varphi$ pieces using the Gauss-Legendre integration rule, where $\cos \theta \in [-1, 1]$ is discretized by N_θ -point Gauss-Legendre quadrature, while $\varphi \in [0, \pi]$ (due to symmetry) is discretized by the Gauss-Legendre quadrature with $N_\varphi/2$ points. $N_B = 20$ (or 10) for each acoustic (or optical) phonon branch, respectively. $N_{dir} = 40 \times 8$ for quasi-1D simulations and $N_{dir} = 32 \times 32$ for quasi-2D or 3D simulations. All numerical results are obtained by a three-dimensional C/C++ program. MPI parallelization computation with 40 – 320 CPU cores based on the decomposition of wave vector space is implemented. In order to reduce the communication times and improve the parallel efficiency, the discrete points corresponding to the specular reflection should be ensured in the same CPU core when the discrete points of the wave vector space are partitioned. The iteration reaches convergence when the difference of the macroscopic variables W between two successive iteration step is smaller than a threshold, for example,

$$\epsilon = \frac{\sqrt{\sum_i^{N_{cell}} (W_i^n - W_i^{n+1})^2}}{\sqrt{\sum_i^{N_{cell}} (W_i^n)^2}} < 10^{-6}, \quad (32)$$

where N_{cell} is the number of discretized cells.

4.1. Quasi-1D heat conduction

4.1.1. Accuracy and efficiency test

Quasi-1D steady heat conduction without external heat source is simulated firstly. System size is L and the temperature at each end side of the system is fixed as T_h and T_c , respectively, where isothermal boundary

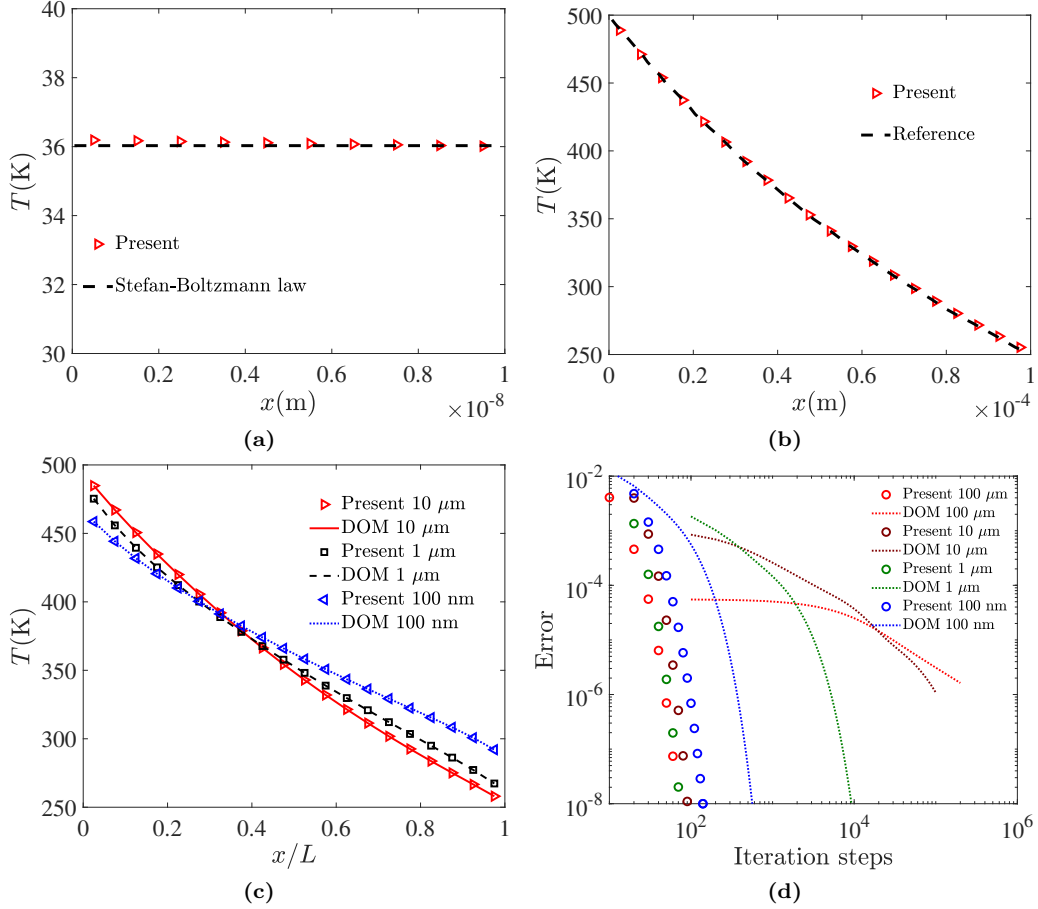


Figure 1: (a) Ballistic regime, $L = 10$ nm, $T_h = 40$ K, $T_c = 30$ K, 10 discretized uniform cells are used. (b,c,d) $T_h = 500$ K, $T_c = 250$ K, 20 discretized uniform cells are used. (b) Diffusive regime, $L = 100$ μm , ‘Reference’ comes from Ref. [40]. A comparison is made between the present scheme and DOM in (c) numerical accuracy and (d) computational efficiency, where ‘Error’ is the difference of the macroscopic heat flux between two successive iteration step. It takes less than 1 second and about 100 iteration steps to reach convergence for the present scheme regardless of the system sizes.

condition is used for the two side of the system. Initial temperature inside the domain is T_c and 40 CPU cores are used.

When $L = 10$ nm, $T_h = 40$ K and $T_c = 30$ K, phonon mean free path is much larger than system size and ballistic phonon transport dominates heat conduction. Phonons emitted from one boundary are absorbed directly by the other boundary without scattering. The specific heat is proportional to T^3 in the low temperature limit so that the temperature in the ballistic limit satisfies Stefan-Boltzmann law [59], i.e., $T^4 = (T_h^4 + T_c^4)/2$. Numerical results in Fig. 1(a) show that the present results well follow the Stefan-Boltzmann law. When $T_h = 500$ K, $T_c = 250$ K and the system size is larger than phonon mean free path, e.g., $L = 100$ μm , as shown in Fig. 1(b), our numerical solutions are in excellent agreement with the reference data which is obtained by solving classical Fourier’s law with the temperature dependent thermal conductivity [40]. Note that when the temperature difference in the domain is large, the thermal conductivity varies with the spatial position so that the temperature distributions are nonlinear. In addition,

20 discretized uniform cells are enough for the present scheme to accurately recover the classical Fourier’s law. When system size decreases from 100 μm to 100 nm, numerical results in Fig. 1(c) show that the present results agree well with the typical DOM. Furthermore, the present scheme significantly reduce the iteration steps compared to the DOM when the system size is large, as shown in Fig. 1(d), where ‘Error’ is the difference of the macroscopic heat flux between two successive iteration step. It takes less than 1 second and tens of iteration steps to reach convergence for the present scheme regardless of the system sizes. Above results show that the present scheme could efficiently describe the heat conduction from the ballistic to diffusive regime.

4.1.2. Selective phonon excitation

Effects of selective phonon excitation on micro/nano scale heat conduction is investigated. Several ways of selective phonon excitation are considered, including ‘only heating LO’, ‘only heating TO’, ‘only heating LA’, ‘only heating TA’, ‘equal heating’ and ‘Joule heating’. ‘equal heating’ represents that p_k in Eq. (2) is equal for all phonon modes. ‘only heating X’ represents that $p_k = 0$ for other phonon branches and p_k is equal for all phonon modes in X branch. In ‘Joule heating’, the energy weights p_k of various phonon modes absorbing from Joule heating in microelectronics are considered, which theoretically results from complicated electron-phonon coupling process. The scattering strengths between electrons with various energy level and phonons with different modes are different and scattering rates depend on the spatial temperature, too. It is better to simultaneously solve the electron and phonon BTE with full scattering kernel. However, it is very expensive and inefficient. Hence some empirical models/parameters or artificial heat source has to be used. In this work, the energy weights are obtained from previous references [9, 29], where 16% of total Joule heating energy is absorbed by ‘LA’, 59% is absorbed by ‘LO’, 4.4% is absorbed by ‘TA’, 20.6% is absorbed by ‘TO’. For phonon modes in the same phonon branch, we assume that p_k is equal.

A Gaussian heat source is implemented inside a quasi-1D system with size L ,

$$\dot{S} = P_{power} \exp\left(-\frac{d}{d_{pump}}\right), \quad (33)$$

where P_{power} is the maximum heat generating power density, d is the distance from the center and d_{pump} is the radius of heat source. Temperature at each end side of the system is fixed as $T_c = 300$ K with isothermal boundary conditions and initial temperature inside the domain is T_c .

Steady thermal transport under different selective phonon excitations, maximum heat generating power density P_{power} , radius of heat source d_{pump} is simulated and half of spatial temperature distributions are plotted in Fig. 2. In order to accurately capture the spatial distribution of heat source, 100 – 200 discretized cells are used. Note that the external heat source continuously heats the system, which results in that the system temperature keeps rising and the phonon scattering rates keep changing during each iteration step, hence theoretically it needs more iterative steps to reach convergence compared with that without external heat source. For all cases, it takes 64 CPU cores, 60 – 140 iteration steps and 5 – 10 seconds to reach

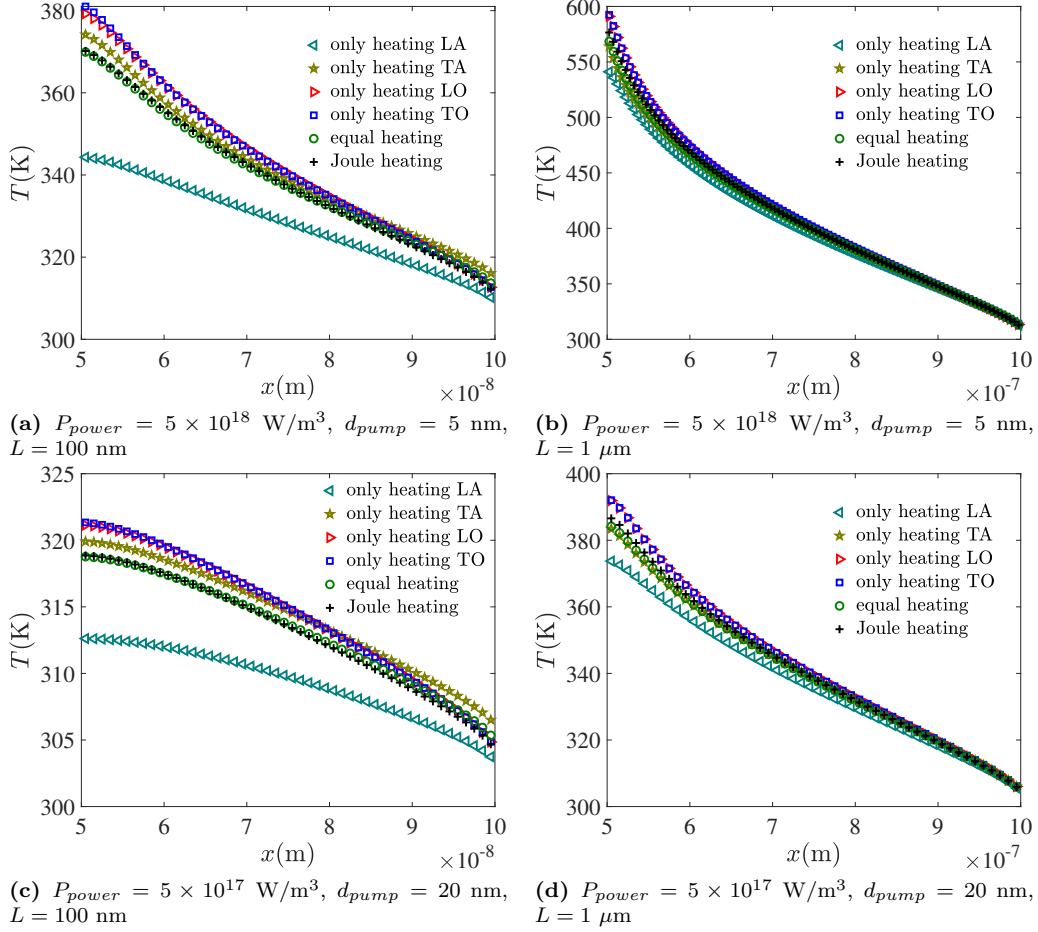


Figure 2: Temperature distributions under different selective phonon excitations, maximum heat generating power density P_{power} , radius of heat source d_{pump} . Half the spatial distribution is drawn due to symmetry.

convergence.

When $L = 100 \text{ nm}$, numerical results in Fig. 2(a,c) show that the temperature rises are different under various selective phonon excitations and large temperature slip appears near the right boundary. Actually when the system size is comparable to or smaller than phonon mean free path, there is insufficient phonon-phonon scattering so that the phonon BTE could be approximated as

$$\mathbf{v}_k \cdot \nabla_{\mathbf{x}} g_k = p_k \dot{S}, \quad (34)$$

$$\implies \mathbf{v}_k (g_k(\mathbf{x}_1 + \mathbf{d}) - g_k(\mathbf{x}_1)) = \int_{\mathbf{x}_1}^{\mathbf{x}_1 + \mathbf{d}} p_k \dot{S}(x') dx', \quad (35)$$

where \mathbf{d} is a distance and \mathbf{x}_1 is the spatial position. Above two equations indicate that when a phonon mode absorbed energy from the external heat source and transferred thermal energy to other spatial domain, the heat dissipation efficiency of this process depends on the phonon group velocity and its absorbed energy in the ballistic regime.

Note that the local temperature is a sum of the phonon distribution function over the wave vector space

so that the temperature rise in the heat source areas depends on the phonon group velocity in the ballistic regime, rather than scattering. The group velocity of LA phonon is large so that its temperature rise is relatively small when the heat source only heats LA phonon. The optical phonon has small group velocity so that the temperature rise of ‘only heating LO’ and ‘only heating TO’ is high. Temperature differences among these three selective phonon excitations (‘Only heating TA’, ‘Only heating TO’ and ‘Only heating LO’) are relatively small. Above results also clarify that the heat dissipations at the micro/nano scale will be more efficient if more external heat source is absorbed and transferred by LA phonons. In addition, the temperature rises of ‘equal heating’ and ‘Joule heating’ are almost the same. That’s because the differences of selective phonon excitation on micro/nano scale heat conduction are mainly reflected in the energy weight absorbed by LA phonons from external heat source based on the results shown in Fig. 2(a). And about 16% heating source energy is absorbed by LA phonons for both ‘equal heating’ and ‘Joule heating’.

When system size increases, it can be found that the temperature distributions under different selective phonon excitation tend to the same in Fig. 2(b,d) and temperature slip near the right boundary decreases. Because when the system size increases, frequent phonon-phonon scattering drives all phonon modes to local equilibrium with the same temperature.

4.2. Heat conduction in a quasi-2D hotspot system

As shown in Fig. 3(a), a heat source with side length H is embedded in the silicon substrate, which is similar to the heat generation and dissipations in a planar MOSFET device. System size of substrate is $L = 5H$ and the bottom is the heat sink with fixed temperature $T_c = 300$ K. Left boundary is symmetric, and the top/right boundary is diffusely reflecting adiabatic boundary. We control the total thermal input power to be equal, and heat generation term is $\dot{S} = 7.1 \times 10^{12}$ W/m³, 7.1×10^{16} W/m³, 7.1×10^{18} W/m³ and $4 \times 7.1 \times 10^{16}$ W/m³ for system size $L = 100$ μm , 1 μm , 100 nm and 50 nm, respectively.

Firstly, heat conduction with ‘Joule heating’ is simulated by the synthetic iterative scheme and the predicted results are compared with the typical DOM or classical Fourier’s law. 50×50 discretized cells are used regardless of system sizes and 320 CPU cores are used for paralleling. From Fig. 3(b), it can be found that when the system size is $L = 100$ nm, the present results are in excellent agreement with the typical DOM and there are temperature slip near the boundaries. When the system size increases, the present scheme has a faster convergence speed compared to the typical DOM, and it is very hard for DOM to quickly converge when the system size is larger than one micron, as shown in Fig. 3(c). It needs more iteration steps compared to the cases in Sec. 4.1. That’s because 1) the relaxation time and specific heat change significantly in each iteration step due to the large heat generation. 2) the temperature at the diffusely/specular reflecting boundaries are unknown and changes with the interior macroscopic distributions in each iteration steps. These input parameters and boundary fields change with the iterative process, which indicates that the targeted discretized equations we numerically solve in each iteration step is changing. When system size is 100 μm (Fig. 3(d)), our results could recover the classical Fourier’s law with bulk

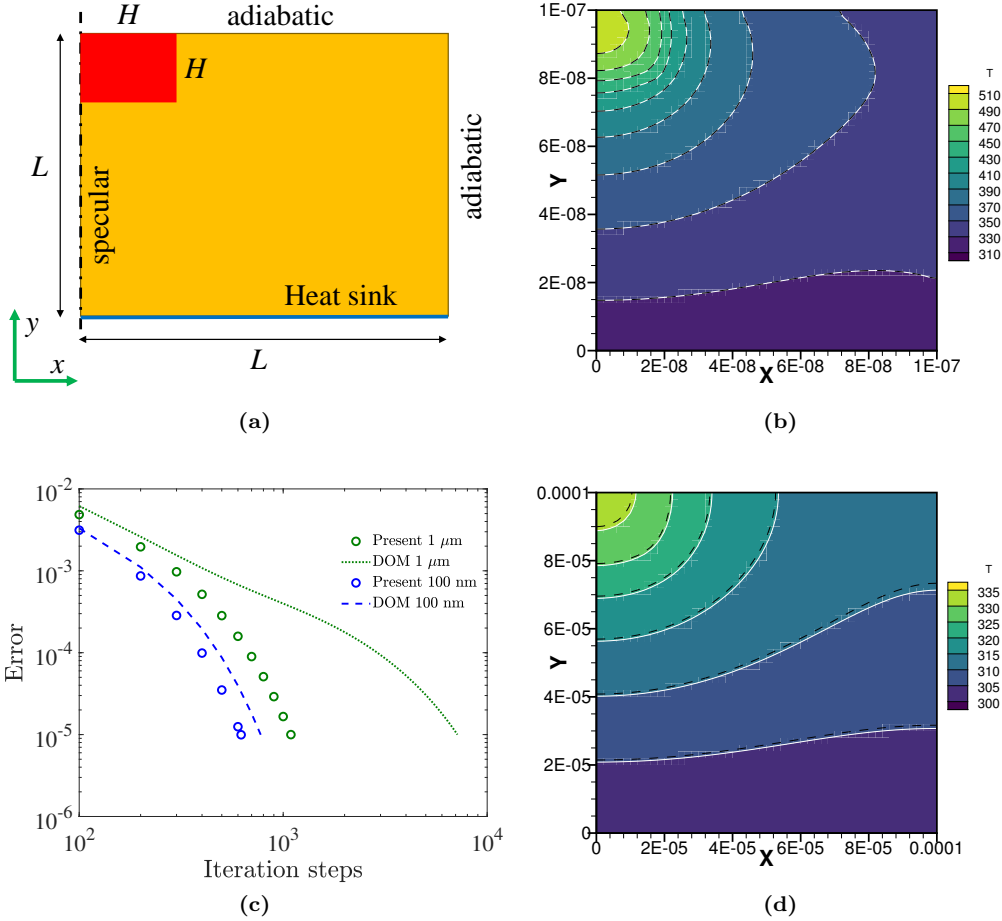


Figure 3: (a) Schematic of a quasi-2D hotspot system. (b) Temperature contour with system size $L = 100$ nm, where the background and white solid line is the present results and the black dashed line is the DOM solution. (c) Convergence efficiency. Iteration is finished when ('Error') the difference of the macroscopic heat flux between two successive iteration step is smaller than 10^{-5} . (d) Temperature contour with system size $L = 100$ μm , where the background and white solid line is the present results and the black dashed line is the solution of classical Fourier's law.

thermal conductivity. These results show that the present scheme could capture the heat conduction from the ballistic to diffusive regime. In the (near) diffusive regime, the present convergence is one to two orders of magnitude faster than the typical DOM.

Secondly, the effects of selective phonon excitation (e.g., 'only heating LA', 'only heating TO', 'equal heating', 'Joule heating') on heat conduction in quasi-2D hotspot system is studied. Basic heat conduction process is shown as follows: when a phonon mode absorbs thermal energy from the external heat source, on one hand, it can transfer energy to other phonon modes at the same geometric location through phonon-phonon scattering, or transfer energy from the heat source region to other geometric regions through ballistic transport. These two energy transfer processes almost occur simultaneously until the phonon energy is completely absorbed by the heat sink at the bottom.

When system size is large enough, sufficient phonon-phonon scattering dominates heat conduction. When

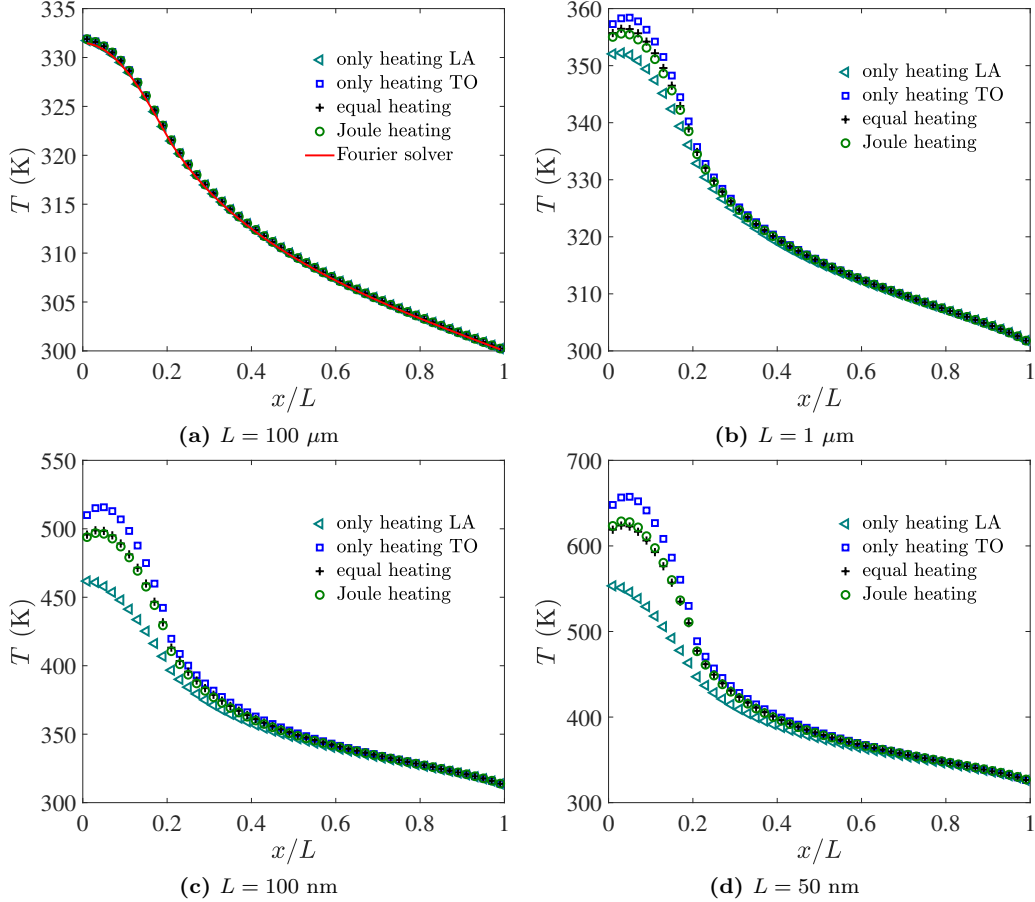


Figure 4: Spatial distributions of the temperature along a diagonal line from the upper left to the lower right with various system sizes.

phonons absorb the thermal energy from the heat source, they will suffer frequent energy exchange with other phonons before they are absorbed by the bottom heat sink. Sufficient energy exchange leads to a similar temperature distribution regardless of selective phonon excitations. Numerical results are in excellent agreement with classical Fourier’s solutions, as shown in Fig. 4(a). When the system size decreases, phonon-phonon scattering becomes insufficient and ballistic phonon transport dominates heat conduction. On one hand, the decreasing system size reduces the effective thermal conductivity, which results in a higher temperature rise. On the other hand, the insufficient phonon-phonon scattering process will allow different phonon modes to transfer energy from the heat source region to the heat sink independently of each other. Note that different phonon modes have different specific heat and group velocity, namely, they have different heat conduction abilities. As can be seen from the numerical results shown in Fig. 4, the temperature rise is smallest when the heat source only heats LA phonons, while it is highest when only heats TO phonons. It indicates that LA phonons have strongest heat conduction ability. In addition, it can be found that the spatial distributions of temperature for ‘equal heating’ and ‘Joule heating’ are almost the same, which is similar to that predicted in the above subsection 4.1.2. The present results can provide a theoretical basis for regulating the heat

dissipation efficiency of semiconductor devices or hotspot systems by selective phonon excitation.

5. Comparison between the effective Fourier’s law and phonon BTE

In this section, thermal dissipations in FinFET/GAAFET structures are simulated, where most of geometrical parameters are obtained from previous references [41, 42, 60, 61]. Discretization of the wave vector space and the parallel computing strategy of the whole solution process are set up in the same way as mentioned in the above section 4. We mainly want to investigate how far the predictions of effective Fourier’s law (1) deviate from the phonon BTE. This research will be of great significance for thermal applications.

Note that the substrate size is larger than $5\ \mu\text{m}$ or tens of microns in some references [25], while there are only hundreds of nanometers in some references [26, 41]. Obviously the peak temperature will be lower and the computational cost will be smaller if the heat sink is closer to the Joule heating areas. In the following simulations, we fixed the substrate size at 200 nm according to the previous paper [41].

5.1. Heat conduction in a quasi-2D vertical cross-section FinFET

Non-Fourier heat conduction in a quasi-2D vertical cross-section FinFET [41] is studied and schematic of geometry is shown in Fig. 5(a). A fin is placed on the top of a substrate, where both height and length of the substrate are $H_{sub} = L_{sub} = 200\ \text{nm}$. The bottom of substrate is a heat sink with isothermal temperature 300 K and its left and right boundaries are symmetric because many FinFETs are arranged on the substrate by periodic arrays. The height and length of fin is $H_{fin} = 100\ \text{nm}$ and $L_{fin} = 162\ \text{nm}$, respectively. Source and drain are placed at the two end side of the fin with length $L_{source} = L_{drain} = 40\ \text{nm}$. Gate length is $L_{gate} = 22\ \text{nm}$, and its position is at the center between source and drain. The heights of source, drain and gate are all $H = 30\ \text{nm}$, and the spacer lengths L_{sp} between source and gate, drain and gate are both 30 nm. Two square heat sinks with edge length $d_{sink} = 22\ \text{nm}$, whose top, left and right boundaries are isothermal boundary conditions with temperature 300 K, are placed directly above the center of the source and drain respectively. Other boundaries of this structure are all diffusely reflecting adiabatic boundary conditions. The external heat source is at the right edge of the gate with power density $\dot{S} = 7.1 \times 10^{18}\ \text{W/m}^3$ [41] and length $L_{hot} = 20\ \text{nm}$.

Three selective phonon excitations are considered, i.e., ‘equal heating’, ‘only heating TO’ and ‘Joule heating’. Non-uniform discretized cells are used and shown in Fig. 5(b). Numerical results with various selective phonon excitation obtained by the present scheme are shown in Fig. 5(c,d,e). It can be found that the temperature rises near Joule heating spot are highest, larger than 150 K. The temperature rises of ‘Only heating TO’ are higher than ‘equal heating’ and ‘Joule heating’, which is in consistent with the results in Fig. 2. [Grid independence testing is conducted in Appendix B and results show that the present discrete settings basically meet the requirements of numerical calculation accuracy and grid independence. In addition, the convergence histories under different selective phonon excitations are also plotted in Fig. B.9\(a\).](#)

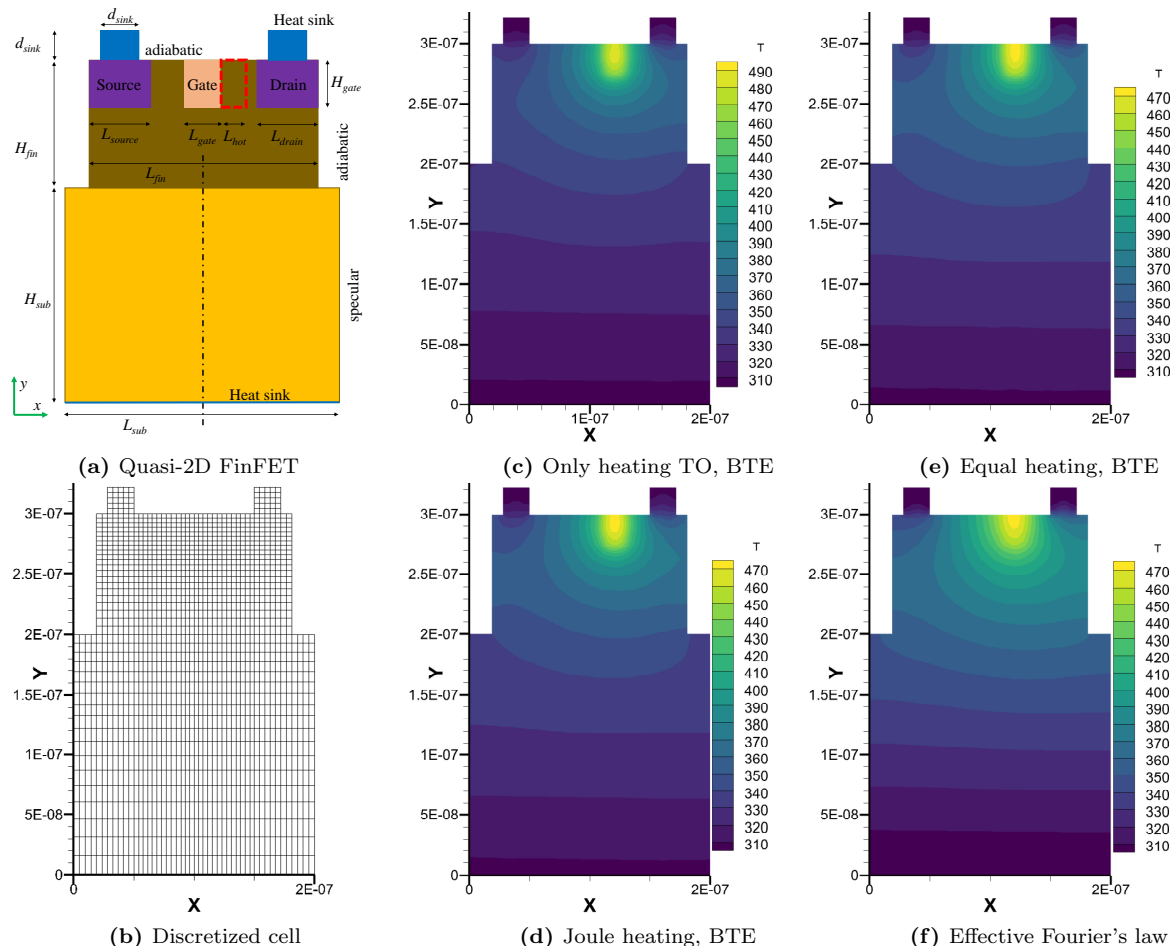


Figure 5: (a) Schematic view of a quasi-2D vertical cross-section FinFET geometry. The Joule heating area is generated at the right edge of the gate with power density $7.1 \times 10^{18} \text{ W/m}^3$. (b) 48×44 non-uniform discretized cells are used for the computational domain. We also simulated the numerical results under a denser grid (grid density in the x direction is 4 times denser and grid density in the y direction is 2 times denser), which is basically no different from the current results. (c-f) Steady temperature distributions predicted by synthetic iterative scheme with (c,d,e) various selective phonon excitation and predicted by (f) the effective Fourier's law with temperature- and size-dependent effective thermal conductivity.

Effective Fourier's law with temperature- and size-dependent effective thermal conductivity

$$\kappa_{eff} = \alpha(\mathbf{x}, L)\kappa_{bulk}(T) = \alpha(\mathbf{x}, L) \times \exp(12.570)/T^{1.326} \quad (36)$$

is also simulated, where $\kappa_{bulk}(T) = \exp(12.570)/T^{1.326}$ is the temperature-dependent bulk thermal conductivity of silicon given in Ref. [40] and α is a dimensionless parameter depends on the spatial position \mathbf{x} or system characteristic length L . Based on previous studies of size effects in room temperature silicon [52, 53], for example, the thermal conductivity of in-plane heat conduction (the length in the other two directions is infinite) at film thickness $100 \mu\text{m}$, 100 nm and 10 nm is $146.0 \text{ W}/(\text{m}\cdot\text{K})$, $57.6 \text{ W}/(\text{m}\cdot\text{K})$, $16.3 \text{ W}/(\text{m}\cdot\text{K})$, respectively. We set $\alpha \approx 10.0/146.0$ in the top square heat sink areas. Considering the similar size of the fins and the substrate areas, we approximately assume that the thermal conductivity of the two regions is equal in the present simulation and $\alpha \approx 30.0/146.0$. Numerical results in Fig. 5(f) show that the temperature rise

predicted by effective Fourier’s law deviates a little from the numerical results of phonon BTE with ‘equal heating’. One of reasons for deviations is that there is no temperature or heat flux slip near the boundaries in the solutions of effective Fourier’s law. Similar thermal distributions predicted by the effective Fourier’s law and phonon BTE show that the macroscopic equations with several empirical coefficients could coarsely capture the micro/nano scale heat conduction in this case.

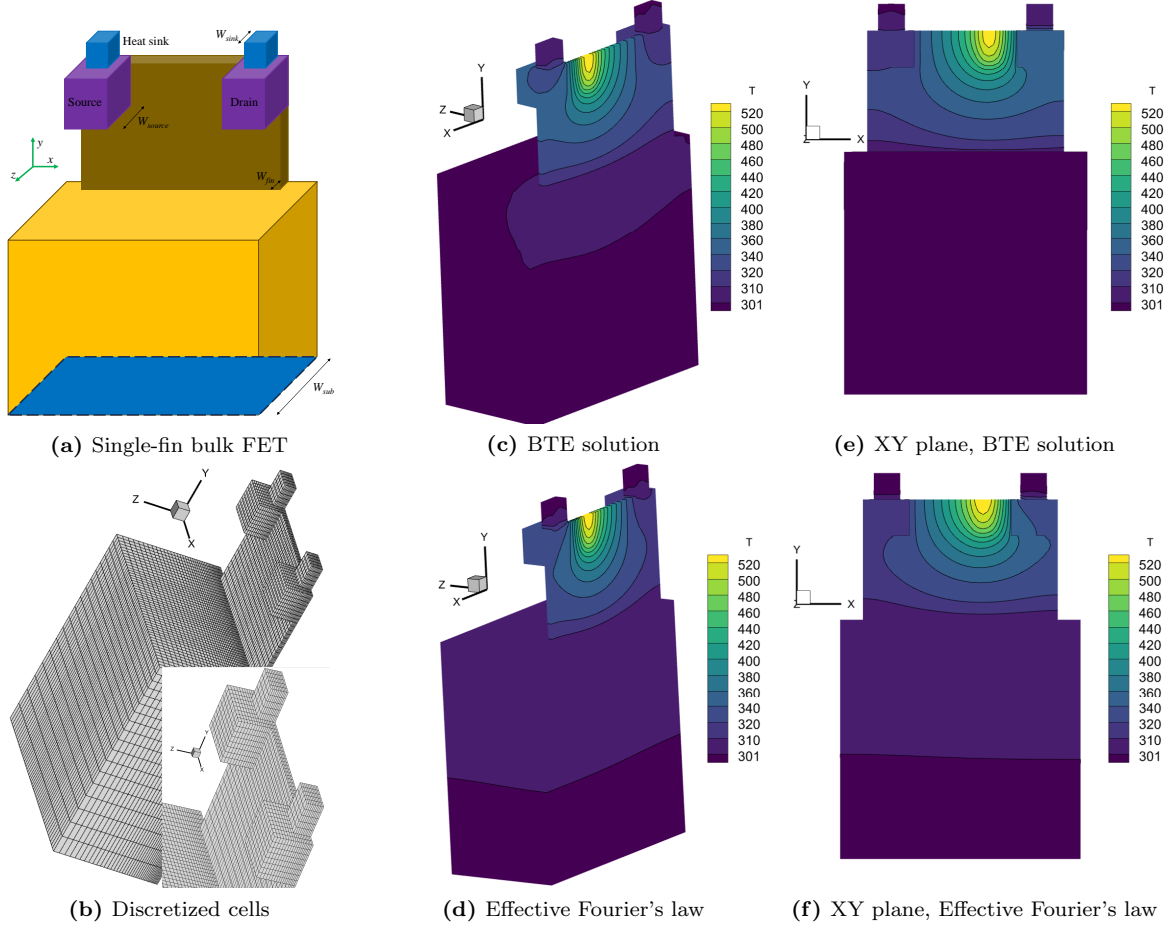


Figure 6: (a) Half of a single-fin bulk FET geometry [41], where the whole back surface of this structure is symmetric. (b) $48 \times 44 \times 39$ non-uniform discretized cells are used for the computational domain. Steady temperature distributions of half of a single-fin bulk FET predicted by (c,d) synthetic iterative scheme and (e,f) effective Fourier’s law.

5.2. Heat conduction in 3D FinFET/GAAFET

Firstly heat conduction in a single-fin bulk FET is simulated. Half of geometry is shown in Fig. 6(a), whose back surface is symmetric. All geometry parameters are the same as those mentioned in previous paper [41]. Geometry sizes in the xy plane are the same as those shown in Fig. 5(a) if looking along the z direction. The widths of fin, source/drain, top heat sink and substrate are $W_{fin} = 4$ nm, $W_{source} = 25$ nm, $W_{sink} = 11$ nm and $W_{sub} = 100$ nm, respectively. The bottom surface of the substrate, front/left/right/top surfaces of the top heat sink are all isothermal boundary conditions with 300 K. The front/left/right surfaces of the

substrate are symmetric. Diffusely reflecting adiabatic boundary conditions are adopted for other surfaces of this structure. The position and power density of the Joule heating zone in the xy plane are the same as that shown in Fig. 5(a), and the width of the Joule heating zone is the same as that of the fin.

In previous studies [41], the maximum temperature in the hotspot region predicted by Monte Carlo method and classical Fourier’s law with bulk thermal conductivity is 493 K and 398 K, respectively, which indicates that the classical Fourier’s law significantly underestimates the peak temperature. Considering that the width of the fin is much smaller than its length and height, the heat conduction in the xy plane will be suppressed by the width, so we set $\alpha = 15.0/146.0$ (36). In other spatial areas, its value is the same as those used in Fig. 5(a). Non-uniform discretized cells are used and shown in Fig. 6(b). Steady temperature distributions are shown in Fig. 6(c-f). It can be found that the temperature rise of the 3D structure is about 50 K higher than that in quasi-2D structure (Fig. 5), which indicates that the smallest fin width affects significantly the hotspot temperature. The temperature rise of substrate is below 2 K and most heat is blocked in the fin areas. In addition, the temperature rise predicted by the effective Fourier’s law is coarsely consistent with the numerical results of BTE although there are some obvious differences in other areas.

Secondly the heat conduction in a double-fin bulk FET [42] structure unit in sub–10 nm advanced technology nodes is studied, as shown in Fig. 7. Front, back, left and right of the whole structure unit are symmetric interfaces, and the whole structure unit is symmetrical about the red dashed line plane. In order to reduce computational cost, only half of the structure unit is calculated because the structure unit is symmetric about the red dashed plane. Detailed geometrical parameters are shown in Table C.3 [62]. Note that the symmetric boundaries are used in the present simulations so that the lengths of source and drain are only a half of real transistors. Gate is at the center of source and drain, and Joule heating area is generated at the right edge of the gate with power density $\dot{S} = 7.1 \times 10^{18}$ W/m³, length $L_{hot} = 4$ nm and same width of the fin. In the following simulations, the heat generation power density is controlled equally, and the steady-state heat dissipation of double-fin bulk FET structure in 10-nm, 7-nm, and 5-nm advanced technology nodes are shown in Fig. 7, where $\alpha = 30/146.0$ in the substrate and 15.0/146.0 in the above the substrate in the numerical solutions of the effective Fourier’s law. When the transistors sizes decreases, the hotspot temperature increases significantly. It can be found that the temperature distributions predicted by BTE is obviously different from the effective Fourier’s law near the hotspot areas and the deviations increase when the transistors sizes decreases. That’s because that the small fin width and close distance between two fins significantly increases the nonlinear relationship between the heat flux and temperature near the connected areas between double fin.

Thirdly heat conduction in a horizontally stacked GAA nanosheet FET structure [60, 61] is studied. Half of a structure unit is shown in Fig. 8(a), where the front, back, left and right of the whole geometry are symmetric interfaces. Geometry parameters are listed in Table C.4. In a structure unit, there are 6 nanosheets with width 25 nm when $2W_{stack} = 23$ nm and 3 nanosheets with width 50 nm when $2W_{stack} = 0$.

The bottom of substrate is the heat sink with isothermal boundary conditions at 300 K and the other boundaries are all diffusely reflecting adiabatic boundary conditions. Gate is at the center of source and drain, and Joule heating area is generated at the right edge of the gate with power density $\dot{S} = 7.1 \times 10^{18}$ W/m³, length 5 nm and same height/width as nanosheets. The three-dimensional temperature contour is shown in Fig. 8, where the effective thermal conductivity is the same as those used in double-fin bulk FET. It can be found that the effective Fourier's law predict a about 10 K higher hotspot temperature than phonon BTE. Main reason of the numerical deviations is highly anisotropic thermal conduction due to the complex stacked typological structures from heat source to heat sink in GAAFET.

These results in this section show that unlike the classical Fourier law which vastly underestimate the peak temperature, the effective Fourier's law is possible to capture the highest temperature rise by empirically adjusting the effective thermal conductivity. However, some local nonlinear thermal conduction phenomena still cannot be accurately described due to the linear assumption of heat flux and temperature gradient. In addition, it is most noteworthy that in engineering thermal applications, how to choose a reasonable effective thermal conductivity coefficient is still a difficult and empirical problem.

6. CONCLUSION

A synthetic iterative scheme is developed for thermal applications in hotspot systems with large temperature variance, where the Newton method is used to deal with the nonlinear relationship between the equilibrium state and temperature. A macroscopic iteration is introduced for preprocessing based on the iterative solutions of the stationary phonon BTE. Macroscopic and mesoscopic physical evolution processes are connected by the heat flux, which is no longer calculated by classical Fourier's law but obtained by taking the moment of phonon distribution function. These two processes exchange information from different scales, such that the present scheme could efficiently deal with heat conduction problems from ballistic to diffusive regime. Numerical results show that the present scheme could efficiently capture the multiscale heat conduction in hotspot systems with large temperature variances. In the (near) diffusive regime, the present convergence is one to two orders of magnitude faster than the typical DOM. The heat dissipation efficiency of silicon-based hotspot systems is high if the external heat source mainly heats the longitude acoustic phonons. In addition, a comparison is made between the solutions of phonon BTE and effective Fourier's law by several heat dissipations problems. Numerical results show that the effective Fourier's law is possible to capture the highest temperature rise by empirically adjusting the effective thermal conductivity. However, some local nonlinear thermal conduction phenomena still cannot be accurately described due to the linear assumption of heat flux and temperature gradient. The present work could provide theoretical guidance for the practical multiscale thermal applications.

Conflict of interest

No conflict of interest declared.

Author Statements

Chuang Zhang: Supervision, Conceptualization, Investigation, Methodology, Numerical analysis, Funding acquisition, Writing - original draft. **Qin Lou:** Methodology, Numerical analysis, Funding acquisition, Writing-review & editing. **Hong Liang:** Conceptualization, Methodology, Numerical analysis, Writing-review & editing.

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Appendix A. Numerical analysis of the present scheme in the diffusive limit

Choose some reference variables, such as reference temperature T_{ref} , velocity v_{ref} , specific heat C_{ref} , system size L_{ref} , and make a dimensionless treatment of phonon BTE,

$$\mathbf{v}_k^* \cdot \frac{\partial g_k^*}{\partial \mathbf{x}^*} = \frac{g_k^{eq,*} - g_k^*}{\text{Kn}_k} + p_k \dot{S}^*, \quad (\text{A.1})$$

where

$$\begin{aligned} \mathbf{v}_k^* &= \frac{\mathbf{v}_k}{v_{ref}}, & g_k^* &= \frac{g_k}{C_{ref} T_{ref}}, & g_k^{eq,*} &= \frac{g_k^{eq}}{C_{ref} T_{ref}}, \\ \text{Kn}_k &= \frac{v_{ref} \tau_k}{L_{ref}}, & \mathbf{x}^* &= \frac{\mathbf{x}}{L_{ref}}, & \dot{S}^* &= \frac{\dot{S} L_{ref}}{C_{ref} T_{ref} v_{ref}} \end{aligned} \quad (\text{A.2})$$

In the diffusive limit, system size is much larger than phonon mean free path and phonon scattering is frequent, so that $\text{Kn}_k \rightarrow 0$.

Firstly, we prove that the phonon BTE could theoretically recover the classical Fourier's law at the non-discrete level in the diffusive limit. Make a Chapman-Enskog expansion of phonon distribution function based on a small perturbation of Kn_k ,

$$g_k^* = g_k^{(0)} + g_k^{(1)} \text{Kn}_k + g_k^{(2)} \text{Kn}_k^2 + \dots \quad (\text{A.3})$$

Equation (A.1) becomes

$$\mathbf{v}_k^* \cdot \frac{\partial}{\partial \mathbf{x}^*} \left(g_k^{(0)} + g_k^{(1)} \text{Kn}_k + g_k^{(2)} \text{Kn}_k^2 + \dots \right) = \frac{g_k^{eq,*} - \left(g_k^{(0)} + g_k^{(1)} \text{Kn}_k + g_k^{(2)} \text{Kn}_k^2 + \dots \right)}{\text{Kn}_k} + p_k \dot{S}^*, \quad (\text{A.4})$$

Based on the zero-order Chapman-Enskog expansion,

$$g_k^* \approx g_k^{(0)} = g_k^{eq,*}. \quad (\text{A.5})$$

Combined with Eqs. (7,8), we can get $T_p = T$ in the diffusive limit, which is consistent with that the frequent scattering leads to a local thermal equilibrium for all phonon modes. Based on the first-order Chapman-Enskog expansion,

$$g_k^{(1)} = p_k \dot{S}^* - \mathbf{v}_k^* \cdot \frac{\partial g_k^{(0)}}{\partial \mathbf{x}^*}, \quad (\text{A.6})$$

$$\implies g_k^* \approx g_k^{eq,*} + \text{Kn}_k \left(p_k \dot{S}^* - \mathbf{v}_k^* \cdot \frac{\partial g_k^{eq,*}}{\partial \mathbf{x}^*} \right), \quad (\text{A.7})$$

$$\implies g_k \approx g_k^{eq} - \tau_k \mathbf{v}_k \cdot \nabla_{\mathbf{x}} g_k^{eq} + \tau_k p_k \dot{S}. \quad (\text{A.8})$$

So that the heat flux in the diffusive limit is

$$\begin{aligned} \mathbf{q} &= \int \mathbf{v}_k g_k d\mathbf{K} \approx - \int \tau_k \mathbf{v}_k \mathbf{v}_k \cdot \nabla_{\mathbf{x}} g_k^{eq} d\mathbf{K}, \\ &= - \int \tau_k \mathbf{v}_k \mathbf{v}_k \cdot \frac{\partial g_k^{eq}}{\partial T} \frac{\partial T}{\partial \mathbf{x}} d\mathbf{K}, \\ &= - \left(\int \tau_k \mathbf{v}_k \mathbf{v}_k C_k d\mathbf{K} \right) \cdot \nabla_{\mathbf{x}} T, \\ &= -\boldsymbol{\kappa}_{\text{bulk}} \cdot \nabla_{\mathbf{x}} T, \end{aligned} \quad (\text{A.9})$$

where C_k is the temperature-dependent specific heat for phonon mode k and $\boldsymbol{\kappa}_{\text{bulk}}$ is the bulk thermal conductivity, which is a second-order tensor. Equation A.9 indicates that the phonon BTE could theoretically recover the classical Fourier's law with temperature-dependent thermal conductivity at the non-discrete level in the diffusive limit [23].

Secondly, the rigorous proof at the discrete level is not an easy task compared to that at the non-discrete level. As reported in previous papers [49, 51], there are a lot of factors that affect the convergence speed and final convergent accuracy at the discrete level, such as spatial discrete schemes, numerical stability, cell size, numerical integration errors, convergence standard, computer truncation error or machine error, boundary conditions and so on. To prove whether a numerical kinetic scheme can recover classical Fourier's law in the diffusive limit at the discrete level, 1) it is necessary to prove that the corresponding discrete BTE is totally in numerically consistent [49] with the discrete Fourier law of thermal conduction equation, 2) it is necessary to prove that it has a high enough computational efficiency in the diffusive limit, 3) discrete time step or cell size cannot be limited by the relaxation time and mean free path, ... For example, the molecular dynamics simulations are accurate, but it is impossible for it to recover the classical Fourier's law in the diffusive limit at the discrete level due to the unaffordable/expensive computational cost and huge statistics errors. Fortunately, a lot of previous studies [50], numerical simulations [54, 52] and Fourier stability analysis [49, 51, 53] have shown that the synthetic iterative scheme has high convergence speed from the ballistic to diffusive regime.

Now Let's do a relatively less rigorous mathematical proof at the discrete level. Note that the final convergent accuracy is totally controlled by the right hand side of Eq. (30) so that the key is to prove that the relationship between the heat flux and temperature at the cell interface follows the Fourier's law at the discrete level. When $\tau_k = 0$, we have $g_{ij,k} = g_k^{eq}(\mathbf{x}_{ij})$ based on Eq. (16), which indicates that the zero-order Chapman-Enskog expansion at the discrete level is satisfied. Next, we need to prove that the first-order Chapman-Enskog expansion at the discrete level is satisfied, too. Based on Eqs. (16,19,31),

$$\begin{aligned}
\mathbf{q}_{ij} &= \sum w_k \mathbf{v}_k g_{ij,k} = \sum w_k \mathbf{v}_k \left(\frac{\tau_k}{\tau_k + \Delta t} g_k(\mathbf{x}_{ij} - \mathbf{v}_k \Delta t) + \frac{\Delta t}{\tau_k + \Delta t} g_k^{eq}(\mathbf{x}_{ij}) \right), \\
&= \sum_{\mathbf{v}_k \cdot \mathbf{n}_{ij} > 0} w_k \mathbf{v}_k \left(\frac{\tau_k}{\tau_k + \Delta t} [g_k^n(\mathbf{x}_i) + \boldsymbol{\sigma}_{i,k} \cdot (\mathbf{x}_{ij} - \mathbf{x}_i - \mathbf{v}_k \Delta t)] + \frac{\Delta t}{\tau_k + \Delta t} g_k^{eq}(\mathbf{x}_{ij}) \right) \\
&+ \sum_{\mathbf{v}_k \cdot \mathbf{n}_{ij} < 0} w_k \mathbf{v}_k \left(\frac{\tau_k}{\tau_k + \Delta t} [g_k^n(\mathbf{x}_j) + \boldsymbol{\sigma}_{j,k} \cdot (\mathbf{x}_{ij} - \mathbf{x}_j - \mathbf{v}_k \Delta t)] + \frac{\Delta t}{\tau_k + \Delta t} g_k^{eq}(\mathbf{x}_{ij}) \right). \tag{A.10}
\end{aligned}$$

In the diffusive limit, $g_k \approx g_k^{eq}$, and the discretized cell size or time step has to be much larger than the phonon mean free path or relaxation time in order to keep fast computational efficiency, i.e.,

$$\Delta t \gg \tau_k, \quad \Delta x \gg |\mathbf{v}_k| \tau_k, \tag{A.11}$$

$$\implies \frac{\Delta t}{\tau_k + \Delta t} \approx 1. \tag{A.12}$$

In addition, the macroscopic and mesoscopic distributions are approximately flat and smooth in the diffusive regime so that

$$g_k^n(\mathbf{x}_i) + \boldsymbol{\sigma}_{i,k} \cdot (\mathbf{x}_{ij} - \mathbf{x}_i - \mathbf{v}_k \Delta t) \approx g_k^n(\mathbf{x}_{ij}) - \boldsymbol{\sigma}_{ij,k} \mathbf{v}_k \Delta t, \quad \mathbf{v}_k \cdot \mathbf{n}_{ij} > 0 \tag{A.13}$$

$$g_k^n(\mathbf{x}_j) + \boldsymbol{\sigma}_{j,k} \cdot (\mathbf{x}_{ij} - \mathbf{x}_j - \mathbf{v}_k \Delta t) \approx g_k^n(\mathbf{x}_{ij}) - \boldsymbol{\sigma}_{ij,k} \mathbf{v}_k \Delta t, \quad \mathbf{v}_k \cdot \mathbf{n}_{ij} < 0. \tag{A.14}$$

Then

$$\begin{aligned}
\mathbf{q}_{ij} &\approx \sum_{\mathbf{v}_k \cdot \mathbf{n}_{ij} > 0} w_k \mathbf{v}_k \left(\frac{\tau_k}{\tau_k + \Delta t} [g_k^n(\mathbf{x}_{ij}) - \boldsymbol{\sigma}_{ij,k} \cdot \mathbf{v}_k \Delta t] + \frac{\Delta t}{\tau_k + \Delta t} g_k^{eq}(\mathbf{x}_{ij}) \right) \\
&+ \sum_{\mathbf{v}_k \cdot \mathbf{n}_{ij} < 0} w_k \mathbf{v}_k \left(\frac{\tau_k}{\tau_k + \Delta t} [g_k^n(\mathbf{x}_{ij}) - \boldsymbol{\sigma}_{ij,k} \cdot \mathbf{v}_k \Delta t] + \frac{\Delta t}{\tau_k + \Delta t} g_k^{eq}(\mathbf{x}_{ij}) \right), \\
&\approx \sum_{\mathbf{v}_k \cdot \mathbf{n}_{ij} > 0} w_k \mathbf{v}_k \left(\frac{\tau_k}{\tau_k + \Delta t} [g_k^{eq,n}(\mathbf{x}_{ij}) - \boldsymbol{\sigma}_{ij,k} \cdot \mathbf{v}_k \Delta t] + \frac{\Delta t}{\tau_k + \Delta t} g_k^{eq}(\mathbf{x}_{ij}) \right) \\
&+ \sum_{\mathbf{v}_k \cdot \mathbf{n}_{ij} < 0} w_k \mathbf{v}_k \left(\frac{\tau_k}{\tau_k + \Delta t} [g_k^{eq,n}(\mathbf{x}_{ij}) - \boldsymbol{\sigma}_{ij,k} \cdot \mathbf{v}_k \Delta t] + \frac{\Delta t}{\tau_k + \Delta t} g_k^{eq}(\mathbf{x}_{ij}) \right), \\
&\approx \sum w_k \mathbf{v}_k [g_k^{eq,n}(\mathbf{x}_{ij}) - \boldsymbol{\sigma}_{ij,k} \cdot \mathbf{v}_k \tau_k] \approx \sum w_k \mathbf{v}_k (-\boldsymbol{\sigma}_{ij,k} \cdot \mathbf{v}_k \tau_k), \\
&\approx - \left(\sum w_k C_{ij,k} \mathbf{v}_k \mathbf{v}_k \tau_k \right) \cdot \nabla T_{ij}, \tag{A.15}
\end{aligned}$$

where

$$\boldsymbol{\sigma}_{ij,k} = \frac{\partial g_{ij,k}}{\partial \mathbf{x}} \approx \frac{\partial g_{ij,k}^{eq}}{\partial \mathbf{x}} = \frac{\partial g_{ij,k}^{eq}}{\partial T} \frac{\partial T_{ij}}{\partial \mathbf{x}} = C_{ij,k} \nabla T_{ij}. \tag{A.16}$$

Above equation (A.15) indicates that the heat flux at the cell interface is proportional to the temperature gradient at the cell interface in the diffusive limit, satisfying discrete Fourier’s law. When Eq. (A.15) is satisfied, we can find that the macroscopic iteration (30) is nearly equivalent to the discrete diffusion equation under the framework of finite volume method.

Appendix B. Grid independence testing

Grid independence testing is conducted in this part and we take quasi-2D vertical cross-section FinFET as an example. Theoretically, it requires more discrete spatial cells and less discrete solid angles in the diffusive regime because the system size is much larger than phonon mean free path and phonon scattering is much frequent. While it requires less discrete spatial cells and more discrete solid angles in the ballistic regime. Results are shown in Fig. B.9, where ‘Joule’ heating is considered. It can be found that there are about 5000 iterative steps to reach convergence. The number of discrete spatial grids (48×44) and discrete solid angles (32×32) used in this paper basically meet the requirements of numerical calculation accuracy and grid independence.

Appendix C. Geometric parameters of FinFET and GAAFET

Geometric parameters of FinFET and GAAFET used in our present simulations are shown in Tables. C.3 and C.4.

Table C.3: Geometrical parameters of a double-fin bulk FET structure unit (Fig. 7) in sub-10 nm advanced technology nodes [42].

Geometry parameters (nm)	Advanced technology nodes		
	10-nm node	7-nm node	5-nm node
Fin length L_{sub}	54	44	36
Fin pitch	34	30	26
W_{sub}	102	90	84
Gate length L_{gate}	18	16	14
Spacer length L_{sp}	7	6	5
$L_{source} = L_{drain}$	11	8	6
Fin width W_{fin}	7	6	5
H	46	46	46
Box height h	50	50	50
H_{sub}	200	200	200

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Table C.4: Geometrical parameters of 3D horizontally stacked GAA nanosheet FETs (Fig. 8).

Symbols	Physical meanings	Size (nm)
L_{sub}	Substrate length	34
H_{sub}	Substrate height	200
W_{sub}	Substrate width	48
$2W_{stack}$	Horizontal distance of nanosheet	0 or 23
H_{sheet}	Thickness of nanosheet	5
W_{sheet}	Width of nanosheet	25
d_{sheet}	Vertical distance of nanosheet	10
L_{gate}	Gate length	12
L_{source} and L_{drain}	Source/drain length	6
H	Source/drain height	45
L_{sp}	Space length between source/drain and gate	5

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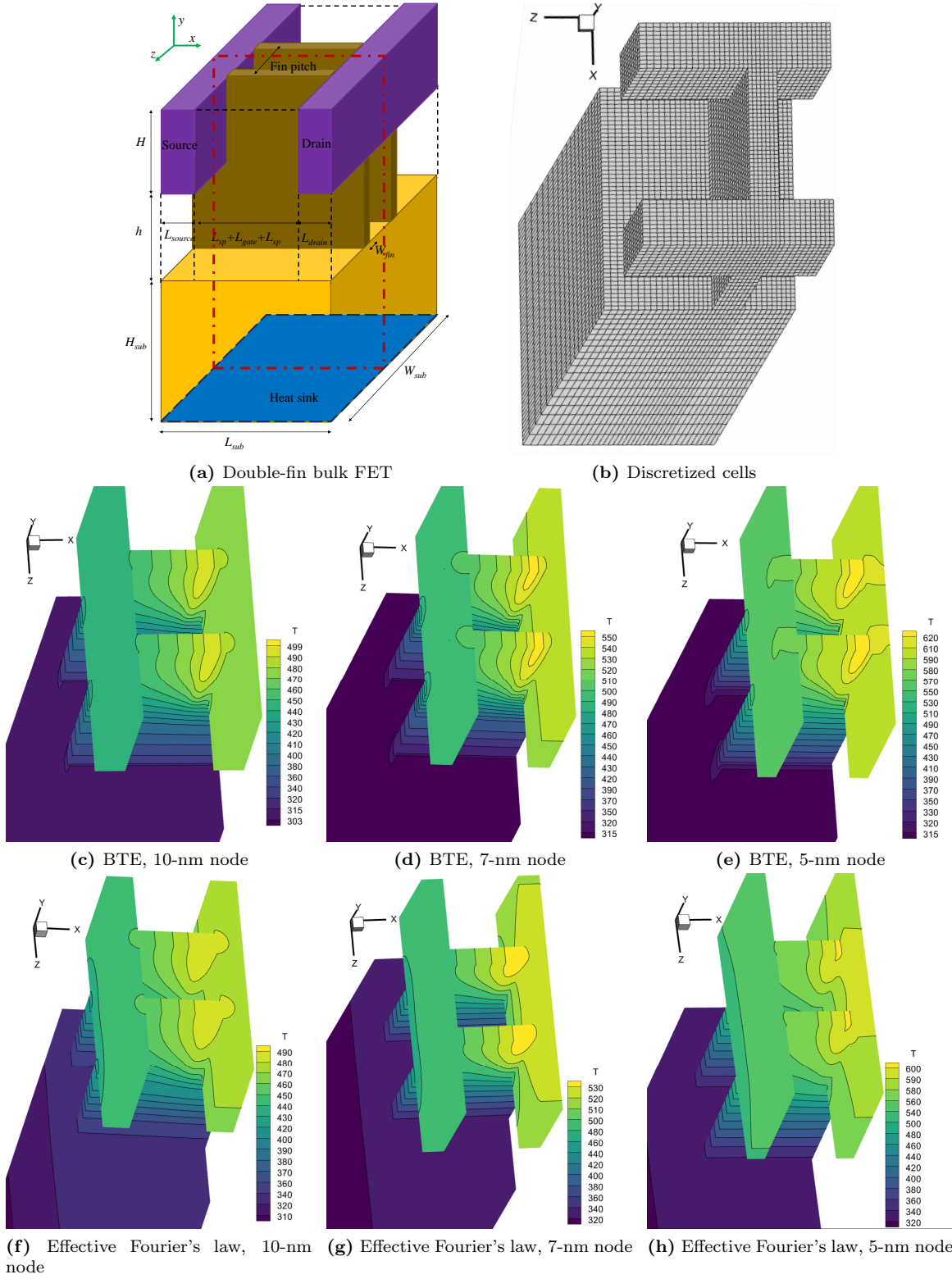
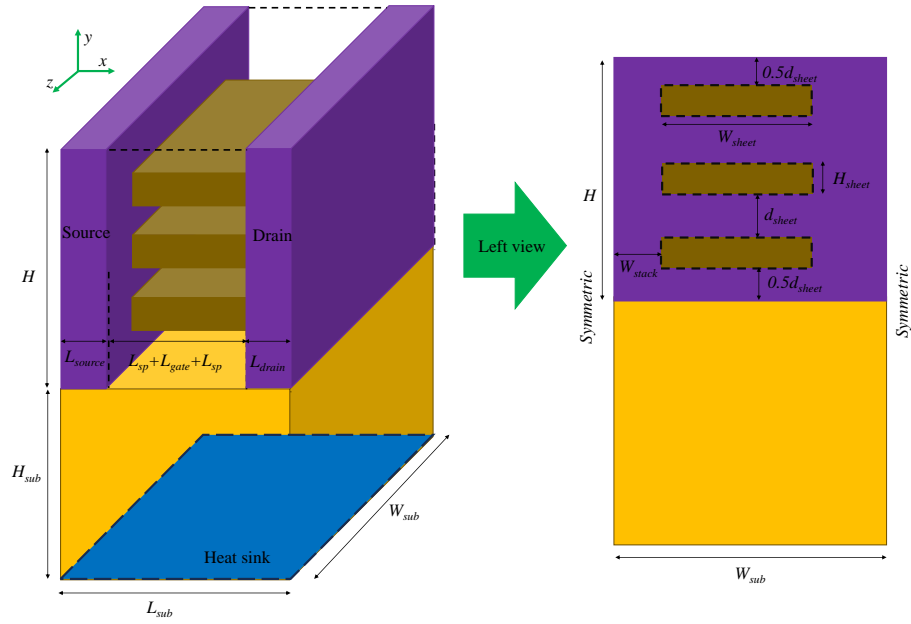
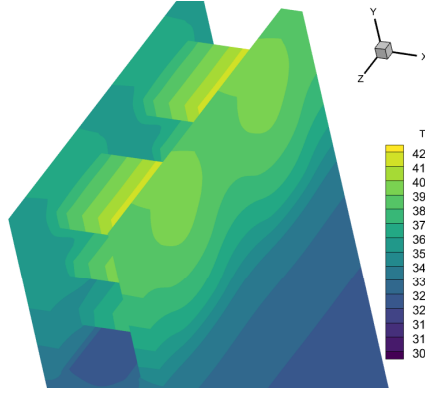


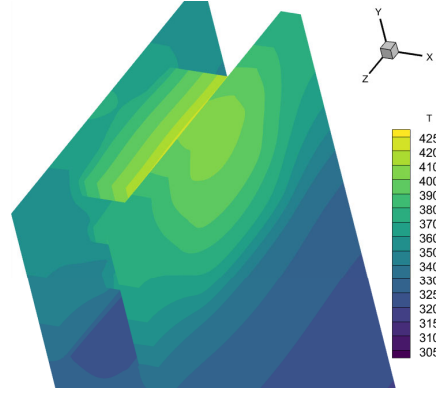
Figure 7: (a) Schematic of a double-fin bulk FET structure unit in sub-10 nm advanced technology nodes. The front, back, left and right of the whole geometric structure unit are symmetric interfaces, and the whole structure unit is symmetrical about the red dashed line plane. (b) Non-uniform discretized cells for half of the structure unit in 7-nm node. Steady temperature distributions of a double-fin bulk FET structure unit predicted by (c,d,e) synthetic iterative scheme and (f,g,h) effective Fourier's law in (c,f)10-nm, (d,g) 7-nm, (e,h) 5-nm advanced technology nodes.



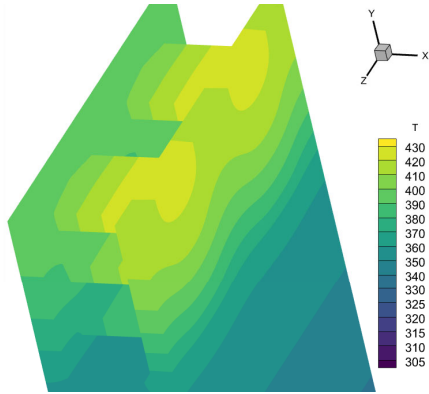
(a) GAAFET



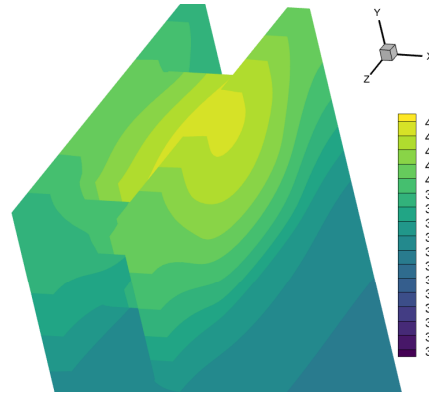
(b) $2W_{stack} = 25$ nm, BTE



(c) $2W_{stack} = 0$, BTE



(d) $2W_{stack} = 25$ nm, Effective Fourier's law



(e) $2W_{stack} = 0$, Effective Fourier's law

Figure 8: (a) Schematic of 3D horizontally stacked GAA nanosheet FETs, where the front, back, left and right of the whole geometry are symmetric interfaces. Steady temperature distributions of 3D horizontally stacked GAA nanosheet FETs predicted by (b,c) synthetic iterative scheme and (d,e) effective Fourier's law.

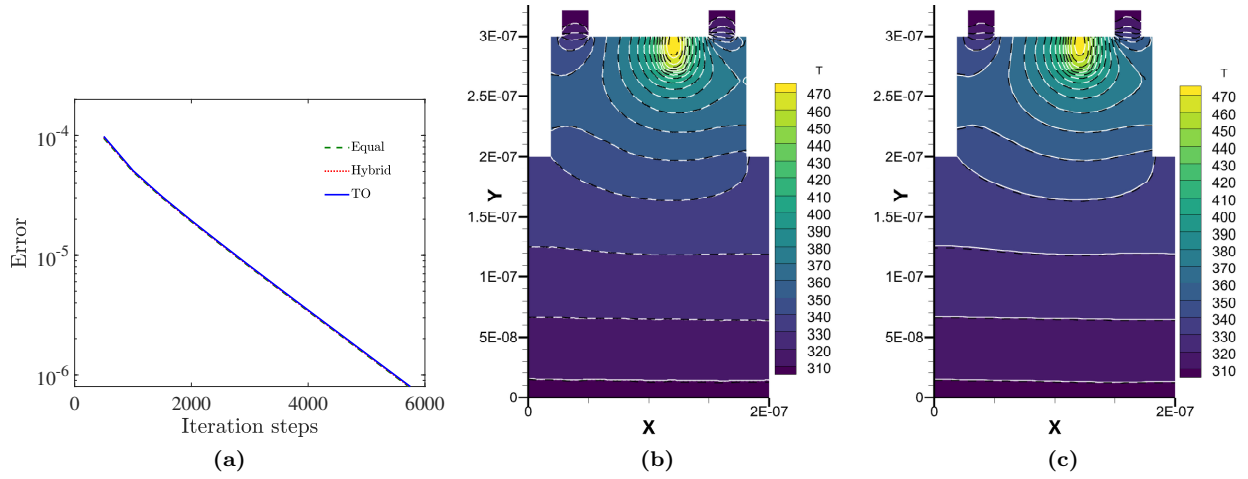


Figure B.9: (a) Convergence history, where Error is the difference of the macroscopic temperature between two successive iteration step. (b) Background and while solid line is the results of denser grid (200×107) and the black dashed line is the results of coarse grid (48×44), where 32×32 discrete solid angles are used. (c) Colored background and white solid line are the results of 64×64 discrete solid angles and the black dashed line is the results of 32×32 discrete solid angles, where coarse grid (48×44) is used.